

LAND DEVELOPMENT | ENGINEERING DESIGN | CONSTRUCTION SERVICES

Geotechnical Report Ramp I-91 NB to Route 5/15 NB over Route 5&15 SB State Project No. 63-703 Hartford, Connecticut

December 12, 2016

Freeman Project No.: 2014-1001

Prepared for: **CME Associates, Inc. 333 East River Drive, Suite 400 East Hartford, CT 06108**

Prepared by:

Freeman Companies, LLC 36 John Street Hartford, CT 06106

> Nathan L. Whetten, P.E., D.GE. Vice President of Geotechnical Services

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1.0 INTRODUCTION

1.1 Summary

This report presents our evaluation of subsurface conditions and geotechnical engineering recommendations for the proposed new bridge, I-91 NB to Route 5/15 NB Ramp over Route 5/15 SB, located in Hartford, Connecticut. The bridge will be an 880 foot-long, 5-span, trapezoidal box steel girder bridge, supported on two abutments and four piers. Abutments will be concrete cantilever with U-type wingwalls. Up to 36 feet of fill will be placed behind Abutment 1 and up to 22 feet of fill will be placed behind Abutment 2. No fill will be place in pier areas.

We recommend that abutments and piers be supported on steel H-Piles driven to refusal on bedrock, and pile tip reinforcement should be provided. Filling behind the abutments and wingwalls will result in settlement of subgrade soils and downdrag loads on piles supporting abutments will occur. We recommend that bitumen coatings be applied to piles supporting the abutments to reduce downdrag loads, or alternatively piles may be oversized to accommodate downdrag loads. Coated piles should be preaugered to the top of the lacustrine deposits to protect the coatings during installation.

Total settlement of fills placed behind abutments and wingwalls is expected to be approximately 2 inches. We recommend that abutments and wingwalls be backfilled with lightweight fill consisting of expanded shale aggregate to reduce settlement to less than 1 inch.

1.2 Scope of Work

Freeman Companies, LLC performed the following tasks:

- Engaged a subsurface exploration contractor to conduct test borings at the site.
- Provided technical monitoring of the explorations.
- Arranged for a testing laboratory to conduct laboratory soil tests.
- Evaluated the subsurface conditions.
- Conducted settlement evaluations.
- Prepared this report containing geotechnical design recommendations and construction considerations.

1.3 Authorization

The work was completed in accordance with our agreement dated October 21, 2015.

1.4 Project Vertical Datum

Elevations in this report are in feet and reference NAVD-88.

2.0 PROJECT AND SITE DESCRIPTION

2.1 Project Description

A new two-lane bridge will carry the I-91 NB to Route 5/15 NB Ramp over Route 5/15 SB, as shown on Figure 1, Site Location Map, and Figure 2, Subsurface Exploration Location Plan. Proposed bridge elements are as follows:

2.2 Site Description

Abutment 1 and Pier 1 will be located on the west side of Route 5/15 SB, south of the off ramp to I-91 SB. The area is grass-covered with some trees. The existing ground surface elevation is about El. 15.

Pier 2 will straddle Route 5/15 SB and the off-ramp to I-91 SB. The east side support will be located between the paved Route 5/15 NB and SB travel lanes and the west side support will be located in the grassy divide between Route 5/15 SB and the I-91 SB off ramp (ground surface approximately El. 21). The existing ground surface elevation is approximately El. 21).

Piers 3 and 4 and Abutment 2 will be located between the paved Route 5/15 NB and SB travel lanes. Ground surface elevations are approximately El. 27 (Pier 3), El. 33 (Pier 4), and El. 38 (Abutment 2).

3.0 EXPLORATIONS

3.1 Recent Explorations

Twelve test borings (S1-1 through S1-12) were drilled by New England Boring Contractors, Inc., Glastonbury, Connecticut, near the proposed abutments and piers to depths ranging from 64 to 100 feet below ground surface. Standard Penetration Tests were completed at maximum 5 foot intervals within the test borings. Ten-foot-long NXsize rock cores were obtained from each boring. Explorations were backfilled with drill cuttings and a pavement patch was placed at ground surface.

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A Freeman Companies engineer monitored the drilling, classified the soil samples, and prepared the test boring logs included in Appendix A, Recent Boring Logs. Exploration locations were surveyed by CME Associates, and are shown on Figure 2, Subsurface Exploration Location Plan.

3.2 Previous Subsurface Explorations

A number of previous test borings were drilled in the vicinity of the new bridge and are considered applicable, including B-158, B-159, and B-188 to B-191. Approximate locations of borings obtained from record documents are shown on Figure 2, Exploration Location Plan, and logs are provided in Appendix B.

3.3 Laboratory Testing

A laboratory testing program was conducted, consisting of:

- \bullet 12 moisture content tests
- \bullet Three pH, electrical resistivity, and soluble sulfate tests
- Nine grain size analyses
- Three Constant Rate of Strain (CRS) Consolidation Tests
- Six Atterberg Limit Determinations
- One unconfined compression test on a rock core sample.

Laboratory tests were conducted by Geotesting Express, of Acton, Massachusetts. Results of laboratory testing are provided in Appendix C, Laboratory Test Data. Results of previous and recent consolidation tests are plotted on Figure 3, Summary of Varved Clay Properties, West of Connecticut River.

4.0 SUBSURFACE CONDITIONS

4.1 Subsurface Conditions

Subsurface conditions encountered in the explorations include Fill, Alluvium, Lacustrine Deposits, and Glacial Till overlying Bedrock as described below. A summary of subsurface data is provided in Table I. Subsurface profiles at the abutments and piers are provided on Figures 4A through 4F, Subsurface Profile.

Groundwater – Water was encountered in the borings at depths ranging from 7 to 20 feet (El 3 to El 22). Groundwater levels were measured during drilling activities and may not represent static levels. Water levels will vary with season, water level in the nearby Connecticut River, precipitation, temperature, and other factors.

Corrosion – Corrosion testing was conducted on samples recovered from test borings S1-2 (Abutment 1), S1-5 (Pier 2), and S1-12 (Abutment 2). Results are summarized below:

5.0 GEOTECHNICAL ENGINEERING RECOMMENDATIONS

5.1 Foundation Design Recommendations

Downdrag – The threshold settlement for downdrag loads on piles is commonly considered to be about 0.4 inches. Settlement evaluations were conducted at the proposed abutments to evaluate the magnitude of total settlement, and whether downdrag loads would occur on piles supporting the abutments due to settlement. Predicted total settlements calculated using the computer program Settle 3D (by RocScience) using normal and lightweight fill are as follows:

Considering the uncertainties in assumptions and parameters, the significant height of fill, and the closeness of estimated geofoam settlement with the threshold settlement for downdrag, use of geofoam for downdrag mitigation is not considered appropriate. We recommend that coatings be applied to piles to reduce downdrag loads, or that piles be oversized to provide additional capacity for downdrag. A 90 percent reduction in downdrag loads is considered feasible using bitumen coatings, whereas a 33 percent reduction in downdrag has been reported for an epoxy coating referred to as *Slickcoat*. We recommend that bitumen coatings be considered for this project. We recommend that backfill at the abutments consist of expanded shale aggregate.

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Corrosion – AASHTO Section 10.7.5 indicates that soils are considered corrosive if pH is less than 5.5, resistivity is less than 2,000 ohmcm, and sulfate concentration is greater than 1,000 ppm. Based on these criteria, soils at the north abutment (S1-12) are marginally corrosive, and soils in other areas are not corrosive. Corrosion mitigation methods include designing piles with sacrificial steel to allow corrosion to occur, providing a protective coating, and other measures (AASHTO C10.7.5). The NCHRP report titled *"Design and Construction Guidelines for Downdrag on Uncoated and Bitumen Coated Piles",* Briaud and Tucker (1996, pg. 10) indicates that bitumen coatings provide corrosion resistance. We recommend the use of bitumen coating at the north bridge abutment to provide both corrosion protection and downdrag mitigation.

Pile Design

- **Seismic Design:** Soils are not susceptible to liquefaction. Soil conditions at the site are defined as AASHTO Site Class D, Stiff Soils. Assume peak ground acceleration (PGA) of 0.061g, a short-term acceleration coefficient $S_{s}= 0.132q$ and long-term acceleration coefficient $S_1 = 0.037q$, respectively.
- **Pile Type:** HP12x74 with pile tip reinforcement driven to end bearing on bedrock, Grade 50 steel. Other H-Pile sections may also be considered.
- **Service Limit:** 125 tons, assumes a HP12x74 pile area equal to 21.76 square inches. Subtract an appropriate allowance for downdrag for piles supporting the abutments, as indicated below.
- **Strength Limit:** For end bearing piles, assume a strength limit equal to the structural capacity of the pile. Settlement of piles is expected to be equal to the elastic compression of the pile.
- **Downdrag:** Estimated downdrag loads are listed below:

Abutment 1:

- 50 tons (single piles, uncoated) or 5 tons (single pile with bitumen coating)
- 4.5 tons (corner pile in a group with bitumen coating)
- 4 tons (side pile in a group with bitumen coating)
- 2.5 tons (inside pile in a group with bitumen coating)

Abutment 2:

115 tons (single piles, uncoated), or 11.5 tons (single pile with bitumen coating)

10.5 tons (corner pile in a group with bitumen coating)

- 9 tons (side pile in a group with bitumen coating)
- 6 tons (inside pile in a group with bitumen coating)
- **Load Tests:** Minimum of 3 dynamic load tests with matching signal analysis (4 tests if 26 or more piles, and no less than 2% of the production piles, AASHTO Table 10.5.5.2.3-3).
- **Test Piles:** Recommend same piles and criteria as load tests (AASHTO 10.7.9)
- • **Minimum Spacing:** Center to center spacing should be 2½ times the pile diameter (AASHTO 2012 10.7.1.2) and at least 30 inches. Minimum 9 inches to the nearest edge of the pile cap
- • **Lateral Resistance:** Use the pile capacity in batter. Lateral load capacities in bending will be provided based on LPile analyses once pile loading is established.
- **Subgrade Preparation Below Pile Cap:** Minimum 12-inch thick layer of crushed stone (CTDOT Form 817 M.01.01 No. 6) overlying separation fabric (CTDOT Form 817 Sec. 7.55 M8.01-26) over the subgrade.
- **Bottom of Structure and Estimated Pile Length:**

6.0 CONSTRUCTION CONSIDERATIONS

6.1 Excavation

Proposed bottom of pile caps will be within the Fill and Alluvium strata. The alluvium and portions of the fill are highly susceptible to disturbance by construction equipment, and are expected to be wet due to shallow groundwater. Excavation to footing subgrade should be made using a smooth-bladed backhoe bucket. Excavation geometries should conform to OSHA excavation regulations contained in 29 CFR 1926, latest edition.

6.2 Pile Cap Subgrade Preparation

The alluvium and portions of the fill have low strength and are highly susceptible to disturbance from construction equipment and vibrations. The contractor shall anticipate that a temporary working pad will be necessary to support installation equipment. We anticipate that working pads could potentially include multiple layers of geogrids, stabilization fabric, crushed stone, well-graded sand and gravel aggregate, or other materials, and the working pad may need to be on the order of three feet thick. The contractor shall be responsible for design of an appropriate working pad capable of supporting his proposed installation equipment. A draft special provision is provided in Appendix D.

Soil bearing surfaces should be protected against freezing both before and after concrete placement. If construction takes place during winter months, foundations should be backfilled as soon as possible following construction. Alternatively, insulating blankets or other methods may be used to protect against freezing.

6.3 Pile Installation

The maximum hammer energy should be determined by a wave equation analysis by the contractor based on the specific hammer characteristics. Test piles and dynamic load testing should be conducted as indicated above. Vibrations from pile driving should not affect the structural integrity of adjacent structures. However, vibration and noise will likely be noticeable inside buildings 300 feet away, or more.

Where bitumen coats are required, coatings should be applied to the piles prior to transportation to the site. It should include a primer coat that may be sprayed or painted onto the piles, and a final coat. A draft special provision for bitumen coatings is provided in Appendix D.

Piles with bitumen coatings should be installed in a preaugered and cased hole to avoid damage to the piles during pile driving. Piles should be preaugered through the existing fill and alluvial deposits (granular soils) to the top of lacustrine deposits. Additionally, the alluvium is expected to be susceptible to settlement from pile driving, and settlement of the alluvial deposits could effect nearby structures and utilities. The top of lacustrine deposits is typically about El -20. Sand should be placed in the casing as the casing is extracted.

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6.4 Expanded Shale Aggregate

Expanded shale aggregate should be placed in layers 1.5 to 2 feet thick, and compacted with self-propelled vibratory compaction equipment with static weight less than 6,600 lbs. The minimum number of passes should be limited to two and the maximum four, to avoid particle breakdown during compaction. A draft special provision is included in Appendix D.

6.5 Temporary Lateral Support

We estimate that excavations on the order of 5 to 8 feet deep will be required to reach pile cap subgrade. Temporary lateral support of excavations will be required to maintain and protect traffic flow, and to protect nearby utilities. Steel sheetpiling or soldier piles and lagging with multiple levels of bracing appears feasible. Surface water should be diverted away from excavations.

6.6 Excavation Dewatering

Excavation dewatering will be required to permit construction in-the-dry. Pumping from sumps located in the bottom of excavations appears feasible. Surface water should be diverted away from excavations. Pumping, handling, and treatment of excavation dewatering fluids should be in accordance with all applicable regulatory agency requirements.

6.7 Reuse of Existing Soils

The existing soils to be excavated will consist primarily of fill and silty sands with gravel. These soils are silty and are not expected to be suitable for reuse as Pervious Structure Backfill or Granular Fill. Excavated soils may be suitable for reuse as embankment fill. However the silty soils are difficult to properly compact when wet, and may need to be dried to achieve compaction. Drying the soils can be difficult and at times impractical, particularly during periods of cold and wet weather.

7.0 FUTURE SERVICES AND LIMITATIONS

We recommend that a qualified geotechnical engineer be engaged during construction to observe:

- Preparation of foundation bearing surfaces
- Pile installation and load tests.
- Verify that soil conditions exposed in excavations are in general conformance with design assumptions, and that the geotechnical aspects of construction are consistent with the project specifications.

This report was prepared for the exclusive use of CME Associates and the project design team. The recommendations provided herein are based on the project information provided at the time of this report and may require modification if there are any changes in the nature, design, or location of the structure.

The recommendations in this report are based in part on the data obtained from the subsurface explorations. The nature and extent of variations between explorations may not become evident until construction. If variations from the anticipated conditions are encountered, it may be necessary to revise the recommendations in this report.

Our professional services for this project have been performed in accordance with generally accepted engineering practices; no warranty, express or implied, is made.

2014-1001New Bridge - Route 5/15 over I-91 NB Contract CORE ID: 15DOT0148AA, State Project No. 63-703 Hartford, Connecticut

Table 1

Notes:

1. Ground surface elevations are at recent test borings were surveyed by CME Associates, Inc. Elevations at previous borings were shown on the logs and converted to NAVD-88.

2. Groundwater levels are approximate

3. Top of bedrock depth is inclusive of weathered bedrock.

4. ">" - Greater Than "--" - Not Encountered (C) - Bedrock Core Taken "NM" - Not Measured

FIGURES

THESE DRAWINGS SHALL NOT BE UTILIZED BY ANY PERSON, FIRM OR CORPORATION WITHOUT THE SPECIFIC WRITTEN PERMISSION OF FREEMAN COMPANIES, LLC

NOTES

 $1.$

PREVIOUS DATA WAS OBTAINED FROM THE REPORT TITLED

BRIDGE AND APPROACHES, HARTFORD-EAST HARTFORD,

CONNECTICUT" DATED MAY 1987.

ADJUSTED FROM NGVD-29.

"GEOTECHNICAL LABORATORY DATA REPORT, CHARTER OAK

2. ELEVATIONS REFER TO NAVD-88. PREVIOUS ELEVATIONS WERE

- **DEFINITIONS**
- COMPRESSION RATIO (= $\Delta \varepsilon / \Delta \text{LOG} \sigma'_{V}$) DURING VIRGIN COMPRESSION **CR** $\overline{}$
	- RECOMPRESSION RATIO (= Ae/LOGo'v) DURING RECOMPRESSION **RR**
	- IN SITU VERTICAL EFFECTIVE STRESS σ'νο
	- PRECONSOLIDATION STRESS σ_P $\overline{}$

SUMMARY OF VARVED CLAY PROPERTIES WEST OF CONNECTICUT RIVER STATE PROJECT NO. 63-703 HARTFORD, CONNECTICUT **FIGURE 3A**

С

LAND DEVELO

ELEVATE YOUR EXPECTATIONS

FIGURE 5

M.K.

 $N.W.$

N.W.

N.T.S.

 $2014 - 1001$ 10/21/2016 **APPENDIX A**

RECENT TEST BORING LOGS

APPENDIX B

PREVIOUS TEST BORING LOGS

 \mathcal{A}

APPENDIX C

RESULTS OF LABORATORY TESTING

Moisture Content of Soil and Rock - AASHTO T 265

Notes: Temperature of Drying : 110º Celsius

Moisture Content of Soil and Rock - AASHTO T 265

Notes: Temperature of Drying : 110º Celsius

Moisture Content of Soil and Rock - AASHTO T 265

Notes: Temperature of Drying : 110º Celsius

pH of Soil by ASTM D4972

Notes: Sample Preparation: screened through #10 sieve Method A, pH meter used

Laboratory Measurement of Soil Resistivity Using the Wenner Four-Electrode Method by ASTM G57 (Laboratory Measurement)

Notes: Test Equipment: Nilsson Model 400 Soil Resistance Meter, MC Miller Soil Box Water added to sample to create a thick slurry prior to testing (saturated condition). Electrical Conductivity is calculated as inverse of Electrical Resistivity (per ASTM G57) Test conducted in standard laboratory atmosphere: 68-73 F
FUGRO CONSULTANTS, INC.

6100 HILLCROFT HOUSTON, TEXAS 77081 PHONE (713) 369-5400 FAX (713) 369-5518

REPORT DATE: 08-01-16

GRO

JOB NUMBER: 04.1115-0003

CLIENT NUMBER:

TIME SAMPLED:

DATE RECEIVED: TIME RECEIVED:

RESULTS OF TESTS

PROJECT: RECONSTRUCTOION OF EXIT CHARTER OAK BRIDGE (GTX 304831)

- FOR: **GEOTESTING EXPRESS, INC. REPORT NUMBER:** 125 NAGOG PARK ACTION, MA 01720 DATE SAMPLED:
- **REPORTED TO: ETHAN MARRO SAMPLED BY: CLIENT**

SOLUBLE SULFATE AASHTO T-290 RECEIVED BY:

SO4CL 069-16

Respectfully submitted,

 *** Dry weight basis**

Steve DeGregorio Chemist

SD

**** WATER EXTRACTION PERFORMED BY USING A 1:10 RATIO OF SAMPLE AND REAGENT WATER FOLLOWED BY CENTRIFUGE AND VACUUME FILTRATION. THE WATER EXTRACT IS THEN ANALYZED USING THE ASTM D-512 AND D-516 METHODS.**

THE RESULTS RELATE AS TO THE LOCATION TESTED AND NO OTHER REFERENCE SHALL BE MADE. THIS REPORT SHALL NOT BE REPRODUCED EXCEPT IN FULL WITHOUT THE WRITTEN APPROVAL OF THE LABORATORY.

Particle Size Analysis - ASTM D422

Sand/Gravel Hardness : ---

Particle Size Analysis - ASTM D422 0.375 in 0.75 in 1.0 in 0.5 in #100 #200 #60 #10 #20 #40 #4 100 90 80 70 60 Percent Finer Percent Finer 50 40 30 20 10 Ω 1000 100 10 10 1 0.1 0.01 0.01 0.001 Grain Size (mm) % Cobble % Sand % Silt & Clay Size % Gravel 5.0 10.3 84.7 --- **Sieve Name** Sieve Size, mm Percent Finer Spec. Percent Complies **Coefficients** $D_{85} = 0.0764$ mm $D_{30} = N/A$ $1.0 in$ 25.00 100 $D_{60} = N/A$ $D_{15} = N/A$ 0.75 in 19.00 95 $D_{50} = N/A$ $D_{10} = N/A$ 0.5 in 12.50 95 0.375 in 9.50 95 $C_u = N/A$ $C_c = N/A$ 4.75 95 $#4$ **Classification** #10 2.00 95 ASTM N/A #20 0.85 94 $\frac{1}{440}$ $\overline{94}$ 0.42 #60 0.25 93 AASHTO Silty Soils (A-4 (0)) #100 93 0.15 #200 0.075 85 **Sample/Test Description**

Sand/Gravel Particle Shape : ---Sand/Gravel Hardness : ---

Particle Size Analysis - ASTM D422 #100 #200 #10 #20 #40 #60 #4 100 90 80 70 60 Percent Finer Percent Finer 50 40 30 20 10 Ω 1000 100 10 10 1 0.1 0.01 0.001 0.001 Grain Size (mm) % Cobble % Sand % Silt & Clay Size % Gravel 0.0 54.9 45.1 --- **Sieve Name** Sieve Size, mm Percent Finer Spec. Percent Complies **Coefficients** $D_{85} = 0.1870$ mm $D_{30} = N/A$ #4 4.75 100 $D_{60} = 0.1051$ mm $D_{15} = N/A$ #10 2.00 100 $D_{50} = 0.0838$ mm #20 0.85 100 $D_{10} = N/A$ #40 0.42 99 $C_u = N/A$ $C_c = N/A$ $#60$ 0.25 97

Classification

Sample/Test Description

ASTM N/A

AASHTO Silty Soils (A-4 (0))

Sand/Gravel Particle Shape : --- Sand/Gravel Hardness : ---

#100 #200

0.15 0.075

76 45

Particle Size Analysis - ASTM D422 #200 #100 #60 #40 \circ #20 #4 100 90 80 70 60 Percent Finer Percent Finer 50 40 30 20 10 $0¹$ 1000 100 10 10 1 0.1 0.01 0.001 0.001 Grain Size (mm) % Cobble % Sand % Silt & Clay Size % Gravel 0.0 16.1 83.9 --- **Sieve Name** Sieve Size, mm Percent Finer Spec. Percent Complies **Coefficients** $D_{85} = 0.0805$ mm $D_{30} = N/A$ #4 4.75 100 $D_{60} = N/A$ $D_{15} = N/A$ #10 2.00 100 $D_{50} = N/A$ $D_{10} = N/A$ #20 0.85 99 #40 0.42 98 $C_u = N/A$ $C_c = N/A$ $#60$ 0.25 96

Classification

Sample/Test Description

ASTM N/A

AASHTO Silty Soils (A-4 (0))

Sand/Gravel Particle Shape : --- Sand/Gravel Hardness : ---

#100 #200

0.15 0.075 94 84

Particle Size Analysis - ASTM D422 #100 #200 #60 #40 #10 #20 #4 100 90 80 70 60 Percent Finer Percent Finer 50 40 30 20 10 $0¹$ 1000 100 10 10 1 0.1 0.01 0.001 0.001 Grain Size (mm) % Cobble % Gravel % Sand % Silt & Clay Size 0.0 28.6 71.4 --- **Sieve Name** Sieve Size, mm Percent Finer Spec. Percent Complies **Coefficients** $D_{85} = 0.1262$ mm $D_{30} = N/A$ #4 4.75 100 $D_{60} = N/A$ $D_{15} = N/A$ #10 2.00 99 $D_{50} = N/A$ $D_{10} = N/A$ #20 0.85 98 95 #40 0.42 $C_u = N/A$ $C_c = N/A$ $#60$ 0.25 93 **Classification** #100 90 0.15 ASTM N/A

Sample/Test Description Sand/Gravel Particle Shape : ---

Sand/Gravel Hardness : ---

#200

0.075

71

Sample/Test Description Sand/Gravel Particle Shape : ---

Sand/Gravel Hardness : ---

Sample Comment: ----

Atterberg Limits - AASHTO T 89 and T 90

Sample Prepared using the WET method

Dry Strength: VERY HIGH Dilatancy: SLOW Toughness: MEDIUM

Atterberg Limits - AASHTO T 89 and T 90

Sample Prepared using the WET method

Dry Strength: HIGH Dilatancy: NONE Toughness: MEDIUM

Sample Comment: ---

Atterberg Limits - AASHTO T 89 and T 90

Sample Prepared using the WET method

Dry Strength: HIGH Dilatancy: SLOW Toughness: MEDIUM

Sample Comment: ---

Atterberg Limits - AASHTO T 89 and T 90

Sample Prepared using the WET method

Dry Strength: HIGH Dilatancy: NONE Toughness: MEDIUM

Atterberg Limits - AASHTO T 89 and T 90

Sample Prepared using the WET method

Dry Strength: HIGH Dilatancy: SLOW Toughness: MEDIUM

Sample Comment: ---

Atterberg Limits - AASHTO T 89 and T 90

Sample Prepared using the WET method

Dry Strength: HIGH Dilatancy: NONE Toughness: MEDIUM

Constant Rate of Consolidation

Constant Strain Rate by ASTM D4186 Summary Report

Constant Rate of Consolidation Constant Strain Rate by ASTM D4186

Pressure Curves

CRC TEST DATA

Note: Specific Gravity and Void Ratios are calculated assuming the degree of saturation equals 100% at the end of the test. Therefore, values may not represent actual values for the specimen.

Constant Rate of Consolidation

Constant Strain Rate by ASTM D4186 Summary Report

Constant Rate of Consolidation Constant Strain Rate by ASTM D4186 Pressure Curves

2500 2000 Excess Pressure, psf
500
500 \bigcirc $-500 -$ 1000 100000 100 10000 $0.4\,$ 0.3 0.2 Pressure Ratio 0.1 0.0 -0.1 $-0.2 -$ 1000 100000 100 10000 Effective Stress, psf

CRC TEST DATA

Note: Specific Gravity and Void Ratios are calculated assuming the degree of saturation equals 100% at the end of the test. Therefore, values may not represent actual values for the specimen.

Constant Rate of Consolidation

Constant Strain Rate by ASTM D4186

Constant Rate of Consolidation Constant Strain Rate by ASTM D4186 Pressure Curves

CRC TEST DATA Project: Reconstruction of Exit Location: Hartford, CT Project No.: GTX-304831 Boring No.: S1-11 Tested By: md Checked By: njh Sample No.: UP-3 Test Date: 06/06/16 Depth: 69-71 ft Test No.: CRC-3 Sample Type: intact Elevation: ---

Soil Description: Moist, reddish brown clay Remarks: System F

Note: Specific Gravity and Void Ratios are calculated assuming the degree of saturation equals 100% at the end of the test. Therefore, values may not represent actual values for the specimen.

Bulk Density and Compressive Strength of Rock Core Specimens by ASTM D7012 Method C

Notes: Density determined on core samples by measuring dimensions and weight and then calculating.

All specimens tested at the approximate as-received moisture content and at standard laboratory temperature.

The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.

Failure Type: 1 = Intact Material Failure; 2 = Discontinuity Failure; 3 = Intact Material and Discontinuity Failure (See attached photographs)

- 1: Best effort end preparation. See Tolerance report for details.
- 2: The as-received core did not meet the ASTM side straightness tolerance due to irregularities in the sample as cored. 3: Specimen L/D < 2.
- 4: The as-received core did not meet the ASTM minimum diameter tolerance of 1.875 inches.
- 5: Specimen diameter is less than 10 times maximum particle size.
- 6: Specimen diameter is less than 6 times maximum particle size.

*Because the indicated tested specimens did not meet the ASTM D4543 standard tolerances, the results reported here may differ from those for a test specimen within tolerances.

UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO ASTM D4543

APPENDIX D

DRAFT SPECIAL PROVISIONS

ITEM #0203xxxA – EQUIPMENT WORKING PAD

Description:

Form 817, Section 203, Structure Excavation shall apply with the following amendments:

Article 2.03.03 – Construction Methods: Insert the following provisions at the end of Item 2, Preparation of Foundations:

The alluvium and portions of the fill have low strength and are highly susceptible to disturbance from construction equipment and vibrations. The contractor shall anticipate that a temporary working pad will be necessary to support installation equipment. Working pads could potentially include multiple layers of geogrids, stabilization fabric, crushed stone, well-graded sand and gravel aggregate, or other materials, and the working pad may need to be on the order of three feet thick. The contractor shall be responsible for design of an appropriate working pad capable of supporting his proposed installation equipment.

ITEM #0702081A- BITUMINOUS COATING FOR STEELPILES

Description: Work under this item shall consist of furnishing and applying bituminous coating to steel piles. This work shall be performed as hereinafter specified, to the dimensions indicated on the plans, or as directed by the Engineer. This work shall also include field applied touch ups to coating damaged during shipping and handling.

Materials: Provide bituminous coating for all piles. Bituminous coating shall consist of canal liner bituminous in accordance with ASTM D 2521. It shall have a softening point of 190°F to 200°F a penetration of 56 to 61 at 77°F and a ductility in excess of 1.38 in. at 77°F. Primer shall be in accordance with AASHTO M 116.

Construction Methods:

- A. All surfaces to be coated with bituminous shall be dry and thoroughly cleaned of dust and loosematerials.
- B. Primer or bituminous shall not be applied in wet weather, nor when the ambient temperature is below 65°F.
- C. Application of the prime coat shall be with a brush or other approved means and in a manner which thoroughly coats the surface of the piling with a continuous film of primer. The primer shall have set thoroughly before the bituminous coating is applied. The bituminous shall be heated to 300°F and applied at a temperature between 200° and 300°F by means of one or more mop coats or other approved means.
- D. The average coating thickness shall be 1/16".
- E. Whitewashing of the coating may be required during hot weather as directed to prevent running or sagging of the asphalt coating prior to driving of the pile.
- F. Bituminous coated piles shall be protected from sunlight or heat immediately after the coating is applied.
- G. The bituminous coating shall not be exposed to damage or contamination during storage, hauling, or handling. Once the bituminous coating has been applied, dragging the piles on the ground or the use of cable wraps around the piles during handling will not be permitted. Pad eyes, or other suitable devices, shall be attached to the piles to be used for lifting and handling.
- H. Where Field splices are required the bituminous coating shall be removed in the splice area. After completing the field splice, the splice area shall be brush coated or mop coated with a minimum of one coat of bituminous material as directed.

Method of Measurement: Bituminous coating will be measured per linear foot of pile coated.

Basis of Payment: Payment shall be made at the contract unit price per linear foot of pile coated. This price shall be full compensation for furnishing all materials, for preparing and placing these materials, and for all labor, equipment tools, and incidentals necessary to complete

ITEM #0702081A

ITEM #0702109A- PRE-AUGERING OF PILES

ITEM #0702111A- DRIVING STEEL PILES

Work under this item shall conform to the requirements of Section 7.02 of Form 817 as replaced by the special provision for Section 7.02 in this contract, amended as follows:

7.02.01- Description: Add the following:

Work under this Item includes pre-augering for piles as indicated on the Plans or as ordered by the Engineer.

7.02.03.2(a) - Construction Methods - Pile Driving Equipment - Hammers: Replace the second paragraph with the following:

The size of hammer shall be adapted to the type and size of piles and the driving conditions. Unless otherwise specified, the minimum rated striking energy per blow for hammers used shall be 26,000-foot pounds (35,000 joules) for driving steel piles. The hammer model used for the driving of test piles shall be used for the driving of service or production piles, unless a change is authorized by the Engineer in writing. Hammers delivering an energy which the Engineer considers detrimental to the piles shall not be used.

7.02.03.2(7) - Construction Methods - Pile Driving Equipment - Pre-Augering: Add the following:

The following apply when pre-auguring is done for piles with bituminous and epoxy coating:

The pre-augered hole is to continue to the top of the clay layer or to the depths shown on the plans or as directed by the Engineer. The pre-augered hole diameter shall be at least the diagonal dimension of the pile, or as directed by the Engineer. All obstructions which could interfere with the driving of piles within the depth of pre-augering are to be removed as part of the pre-auguring work.

The Contractor shall provide temporary casing to maintain the pre-augured dimension of the hole. Upon completion of pile driving, the annulus between the pile and outer hole diameter shall be filled with clean sand and any temporary casing will be removed.

7.02.05.11 - Basis of Payment - Pre-Augering of Piles: Add the following:

This work shall also include obstruction removal, casing, and sand backfill

ITEM #0207150A - LIGHTWEIGHT FILL

Description: Work shall consist of furnishing and placing lightweight fill in the formation of embankments or as backfill in front of and behind structures. This work shall be performed as hereinafter specified, to the dimensions indicated on the plans, or as directed by the Engineer. This item shall also consist of furnishing and placing crushed stone or gravel in burlap bags at the inlet ends of weep holes in structures to the dimensions indicated on the plans or as ordered by the Engineer.

Materials: Lightweight fill shall be a rotary kiln expanded shale aggregate meeting the requirements of ASTM C 330. No by-product slags, cinders or by-products of coal combustion shall be permitted. The aggregate shall consist of tough, durable, non-corrosive particles with the following gradation:

The dry loose unit weight shall be less than 50 pounds per cubic feet (pcf). The lightweight aggregate supplier shall submit verification of an in-place compacted total unit weight (by methods defined in AASHTO T99) of less than 65 pcf. For purposes of this specification, the total unit weight is defined as the maximum dry density multiplied by one plus the moisture content (as a decimal). For example, if the maximum dry density is 45 pcf and the moisture content is 9%, the total unit weight is 49 pcf.

The maximum soundness loss when tested with 5 cycles of magnesium sulfate shall be 10 percent (ASTM C 88). The maximum Los Angeles Abrasion loss when tested in accordance with ASTM C 131 (B grading) shall be 40 percent.

The lightweight aggregate producer shall submit verification that the angle of internal friction is equal to or greater than 40 degrees when measured in a triaxial compression test on a laboratory sample with a minimum diameter of 250mm.

The materials for bagged stone shall conform to the following requirements: the crushed stone or gravel shall conform to the grading requirements of Article M.01.01 for No. 3 or No. 4 coarse aggregate or a mixture of both; the bag shall be of burlap and shall be large enough to contain one cubic foot of loosely packed granular material. Construction Methods: When applicable and except where noted below, lightweight fill placement shall conform to the requirements of Sections 2.02.03 and 2.16.03 of the Standard Specifications, Form 817.

The lightweight fill shall be placed in layers of a thickness of 1.5 ft to a maximum of 2.0 ft. Each layer shall be compacted by the use of self-propelled vibratory compaction equipment with static mass (weight) less than 6,600 lbs. The minimum number of passes shall be two (2) and the maximum four (4). The actual lift thickness and exact number of passes shall be determined by the Engineer depending on the type of compaction equipment. The contractor shall take all necessary precautions during construction activities in operations on or adjacent to the lightweight fill to ensure that the material is not over compacted. Construction equipment, other than for compaction, shall not be operated on the exposed lightweight fill.

Where weep holes are installed within the limits of the lightweight fill, bagged stone shall be placed around the inlet end of each weep hole, to prevent movement of the lightweight fill material into the weep hole. Approximately one cubic foot of crushed stone or gravel shall be enclosed in each of the burlap bags. All bags shall then be securely tied at the neck with cord or wire so that the enclosed material is contained loosely. The filled bags shall be stacked at the weep holes to the dimensions shown on the plans or as directed by the Engineer. The bags shall be unbroken at the time lightweight fill material is placed around them and bags which are broken or burst prior to or during the placing of the lightweight fill material shall be replaced at the expense of the contractor.

Method of Measurement: Lightweight fill shall be measured in place after compaction, including allowances for settlement. There shall be no direct payment for bagged stone, but the cost thereof shall be considered as included in the cost of the work for "Lightweight Fill".

Basis of Payment: This work will be paid for at the contract unit price per cubic yard for "Lightweight Fill", complete in place, which price shall include all materials, transportation, tools, equipment and labor incidental thereto.

Pay Item Lightweight Fill **Pay Unit** c.y.

LAND DEVELOPMENT | ENGINEERING DESIGN | CONSTRUCTION SERVICES

Geotechnical Report Bridge 00480, I-91 over Airport Road Relocation of I-91 NB Interchange 29 and Widening of I-91 NB and Rt. 15 and I-84 EB State Project No. 63-703 Hartford, Connecticut

December 28, 2016

Freeman Project No.: 2014-1001

Prepared for: **CME 333 East River Drive Suite 400 East Hartford, CT 06108**

Prepared by:

Freeman Companies, LLC 36 John Street Hartford, CT 06106

> Nathan L. Whetten, P.E., D.GE. Vice President of Geotechnical Services

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1.0 INTRODUCTION

1.1 Summary

This report presents our evaluation of subsurface conditions and geotechnical engineering recommendations for the proposed improvements to Bridge 00480. The bridge carries Interstate 91 over Airport Road in Hartford, Connecticut.

The proposed improvements include widening the bridge on the northbound (east) side by 14 feet. We recommend that the bridge be supported on drilled micropiles socketed into bedrock to avoid critical utilities located within the proposed widening. Our detailed foundation design recommendations follow.

1.2 Scope of Work

Freeman Companies, LLC performed the following tasks:

- Engaged a subsurface exploration contractor to conduct test borings at the site.
- Provided technical monitoring of the explorations.
- Arranged for a testing laboratory to conduct laboratory soil tests.
- Evaluated the subsurface conditions and prepared this report containing geotechnical design recommendations and construction considerations.

1.3 Authorization

The work was completed in accordance with our agreement dated October 21, 2015.

1.4 Project Vertical Datum

Elevations in this report are in feet and reference NAVD-88. Contract documents for the existing bridge reference NGVD-29. To convert elevations in NGVD-29 to NAVD-88, subtract 0.86 feet.

2.0 SITE AND PROJECT DESCRIPTION

2.1 Site Description

Bridge 00480 carries I-91 over Airport Road. I-91 Northbound has three travel lanes with breakdown lanes on each side. I-91 Southbound has three travel lanes, a right side off-ramp, and breakdown lanes on each side. Airport Road has two travel lanes in each direction. Bridge grade is about El. 31; Airport Road grade is about El. 14.

Several utilities are located close to the bridge. Two 68-inch by 106-inch elliptical RCP pipes extend southwest toward the bridge from a drainage ditch (wetland) located northeast of the bridge, and are carried beneath the bridge above a water line in a junction box. A 36-inch diameter water main runs beneath the bridge parallel to Airport Road. Telephone and electrical utilities are also present.

2.2 Existing Bridge

Existing bridge parameters are as follows:

2.3 Proposed Modifications

Bridge 00480 will be widened by 14 feet on the Northbound (east) side. The proposed widening will provide a fourth travel lane. Abutments will be extended on the Northbound side to support the widened bridge. The proposed widening must avoid the various utilities that run beneath the bridge.

The proposed widening will require approach embankment fills on the Northbound side. Proposed slopes range from 2 horizontal to 1 vertical (2H:1V) in areas where there is sufficient space to place embankment fill, to 1.5H:1V due to wetlands at the toe of slope or limited Right-of-Way. Embankment slopes are discussed in a separate report.

3.0 EXPLORATIONS

3.1 Recent Explorations

Recent explorations included two test borings (S-480-1, S-480-2) and one Cone Penetrometer Test (CPT480-1) conducted May 9 to 10, 2016, and on June 13, 2016, respectively. The test borings were drilled by New England Boring Contractors, Inc., of Glastonbury, Connecticut, and the Cone Penetrometer Test (CPT) was conducted by ConeTec, of West Berlin, New Jersey. Test borings were drilled adjacent to the north and south abutments on the east side; the CPT was drilled in the median of Airport Road on the east side of the bridge. Exploration locations were surveyed by CME Associates, and are shown on Figure 2, Subsurface Exploration Location Plan.

Test borings S-480-1 and S-480-2-OW were drilled to depths of 59 to 59.5 feet below ground surface. Standard Penetration Tests were conducted at maximum 5 foot intervals and two five-foot-long NX-size rock core samples were recovered from each boring. Boring S-480-1 was backfilled with drill cuttings. Boring S-480-2 OW was backfilled with well materials and a roadway box was placed at ground surface to protect the installation.

CPT-480-1 was drilled to a depth of 42.5 feet below ground surface. The CPT was advanced using standard CPT push techniques, and the subsurface data was recorded continuously by a piezocone mounted on the tip.

A Freeman Companies geologist monitored the drilling, described the soil samples, and prepared the test boring logs included in Appendix A, Recent Exploration Logs. The CPT log prepared by ConeTec is also included in Appendix A.

3.2 Previous Subsurface Explorations

Several previous test borings, B-22 through B-25 were drilled for Bridge 00480, and are applicable to the proposed widening. Boring logs are shown in profile on the contact drawings in Appendix B, Previous Explorations.

3.3 Laboratory Testing

A laboratory testing program was conducted, consisting of:

- Two pH tests, two electrical resistivity tests, and two soluble sulfate tests
- One grain size analysis
- One unconfined compression test on a rock core sample.

Laboratory tests were conducted by Geotesting Express, of Acton, Massachusetts. Results of laboratory testing are provided in Appendix C, Results of Laboratory Testing.

4.0 SUBSURFACE CONDITIONS

4.1 Subsurface Conditions

Subsurface conditions encountered generally consist of sand and silt, Varved Clay, and Glacial Till overlying bedrock as described below. A subsurface profile along the proposed structure is shown on Figure 3, Subsurface Profile. Subsurface data are summarized on Table I included at the end of the report.

Groundwater – Water was encountered in the borings at depths ranging from 0 to 13 feet, corresponding to El 2 to El. 10. However, groundwater levels were measured during drilling activities and may not represent static levels. Observation well S-480-2 OW was dry at 13.7 feet (El. 1.1) five months after the well was installed. This measurement was made following a period of relatively dry weather. Water levels will vary with season, water levels in the nearby Connecticut River, precipitation, temperature, and other factors.

Corrosion – Corrosion testing was conducted on samples recovered from test borings S-480-1 (Abutment 1) and S-480-2 OW (Abutment 2). Results are summarized below:

Soil with a pH value lower than 5.5, or soil with electrical resistivity less than 2,000 ohm-cm, or sulfates greater than 1,000 ppm is considered to be a "potential pile deterioration or corrosion situation" per AASHTO 10.7.5.

5.0 GEOTECHNICAL ENGINEERING RECOMMENDATIONS

5.1 Recommended Soil Properties

(1) Undrained strength relationships were determined by laboratory testing in a previous report prepared by Haley & Aldrich titled *"Geotechnical Laboratory Data Report, Charter Oak Bridge and Approaches, Hartford-East Hartford, Connecticut, State Project No. 63-384"*, dated May 1987.

Bedrock is assumed to have a total unit weight of 160 pounds per cubic foot and an unconfined compression strength of 8,000 pounds per square inch based on the results of laboratory testing.

5.2 Foundation Design Recommendations

The existing bridge is supported on Steel H-Piles. Considering the various utilities in the vicinity of the proposed widening, we recommend that the bridge widening be supported on micropiles drilled into bedrock. Design recommendations are provided below:

- **Footings or Pile Cap Foundation Depth:** Minimum of 4 feet below the lowest adjacent ground surface.
- **Backfill Material:** Pervious Structure Backfill (CTDOT Form 817 M.02.05) behind the abutments and abutment wingwalls. Place above a line defined by a 1V:1.5H slope extending up from the heel of the footing to grade.
- **Weep Holes:** 4 inch dia. weep holes at max 10 foot spacing, installed according to CTDOT specifications.
- **Lateral Earth Pressures:** Refer to Figure 4 Active Earth Pressures
- **Seismic Design:** Soils are not susceptible to liquefaction. Soil conditions at the site are defined as AASHTO Site Class D, Stiff Soils.
- **Micropile Design:** Design micropiles with a 10-inch diameter bonded zone socketed into bedrock. Design Micropiles as Type A.
- **Corrosion Protection:** Soils are considered corrosive per AASHTO 10.7.5. Provide double corrosion protection (bar surrounded by grout covered by plastic sheath surrounded by grout).
- **Strength Limit Axial Compression:** 576 kips assuming a grout-to-rock bond strength of 11 ksf, and a 20-foot-long bonded length in rock. The low estimated bond strength reflects the low RQD values in the rock cores. Other capacities can be obtained by shortening or lengthening the bonded length
- **Service Limit** (**Allowable) Axial Compression:** 290 kips, assuming a grout-to-rock bond strength of 11 ksf, a 20-foot-long bonded length in rock, and a resistance factor of 0.5 (AASHTO Table 10.5.5.2.5-1)
- **Minimum Spacing:** Minimum 30 inches or 3 times the pile diameter, whichever is greater (AASHTO 10.9.1.2)
- **Settlement:** Maximum total settlement of micropile is estimated at less than ¼ inch. This settlement will occur during construction. Settlement due to filling behind the widened abutment is also expected to result in less than ¼ inch. This settlement is not sufficient to trigger downdrag loads on piles.
- **Load Tests:** We recommend that a minimum of two load tests be required for this project, one at each abutment.
- **Lateral Resistance:** Install micropiles in batter where needed to resist lateral loads. Additional lateral loading in bending will be provided once pile loading has been established. For a micropile with a 9.625-inch O.D. outer casing and a No. 28 central rebar, the following lateral loads and deflections were calculated using the computer program L-Pile. Results are presented in Appendix D.

- **Drilling:** Use casing through soil.
- **Subgrade Preparation Below Pile Cap:** Recommend minimum 12-inch thick layer of crushed stone overlying separation fabric over the subgrade.
- **Approach Slab:** Recommended to reduce abrupt transition from earth to pile support.
- **Estimated Pile Length:** Estimated lengths are provided in the table below:

6.0 CONSTRUCTION CONSIDERATIONS

6.1 Excavation

Conventional excavation equipment appears practical for excavation. Excavation geometries should conform to OSHA excavation regulations contained in 29 CFR 1926, latest edition.

6.2 Micropile Installation

We recommend that micropiles be drilled with a temporary casing. Micropile drilling equipment must be capable of drilling through the overburden which includes glacial till, and be capable of penetrating through fractured and intact bedrock. Drilling techniques should limit loss of ground. During casing removal, the casing should remain full of grout to limit the potential for drill hole collapse. Contractors should expect that tremie placement of grout will be required.

6.3 Pile Cap Bearing Surface Preparation

Excavated subgrades for the pile cap should be covered with separation fabric and crushed stone placed over the fabric, and then proofrolled with a vibratory plate compactor. If the subgrade beneath the crushed stone is found to be excessively soft or yielding, it may be necessary to overexcavate the soft material and place additional crushed stone over fabric. If vibratory proof compaction of the subgrade proves detrimental due to the presence of groundwater, static rolling may be allowed at the discretion of the Engineer.

Soil bearing surfaces should be protected against freezing both before and after concrete placement. If construction takes place during winter months, foundations should be backfilled as soon as possible following construction. Alternatively, insulating blankets or other methods may be used to protect against freezing.

6.4 Temporary Lateral Support

We estimate that excavations will be required to reach the pile cap subgrade. Temporary lateral support of excavations will be required to maintain and protect traffic flow, and to protect nearby utilities. Steel sheetpiling or soldier piles and lagging with multiple levels of bracing appears feasible. Surface water should be diverted away from excavations.

6.5 Excavation Dewatering

Excavation dewatering will be required to permit construction in in-the-dry. Pumping from sumps located in the bottom of excavations appears feasible. Surface water should be diverted away from excavations. Pumping, handling, and treatment of excavation dewatering fluids should be in accordance with all applicable regulatory agency requirements.

6.6 Reuse of Existing Soils

The existing soils to be excavated will consist primarily of fill and silty sands with gravel. These soils are silty and are not expected to be suitable for reuse as Pervious Structure Backfill or Granular Fill. Excavated soils may be suitable for reuse as embankment fill. However, the silty soils are difficult to properly compact when wet, and may need to be

dried to achieve compaction. Drying the soils can be difficult and at times impractical, particularly during periods of cold and wet weather.

7.0 FUTURE SERVICES AND LIMITATIONS

We recommend that a qualified geotechnical engineer be engaged during construction to observe:

- Preparation of foundation bearing surfaces
- Pile installation and load tests
- Verify that soil conditions exposed in excavations are in general conformance with design assumption, and that the geotechnical aspects of construction are consistent with the project specifications.

This report was prepared for the exclusive use of CME Associates and the project design team. The recommendations provided herein are based on the project information provided at the time of this report and may require modification if there are any changes in the nature, design, or location of the structure.

The recommendations in this report are based in part on the data obtained from the subsurface explorations. The nature and extent of variations between explorations may not become evident until construction. If variations from the anticipated conditions are encountered, it may be necessary to revise the recommendations in this report.

Our professional services for this project have been performed in accordance with generally accepted engineering practices; no warranty, express or implied, is made.

FIGURES

2014-1001 Rehabilitation of Bridge 00480, I-91 over Airport Road Contract CORE ID: 15DOT0148AA, State Project No. 63-703 Hartford, Connecticut

Table 1 Subsurface Data

Notes:

1. Ground surface elevations at recent test borings were surveyed by CME Associates, Inc. Ground surface elevation at previous borings were shown on the logs and corrected to NAVD-88 on this table.

2. Groundwater levels are approximate.

3. Top of bedrock depth is inclusive of weathered bedrock.

4. ">" - Greater Than "--" - Not Encountered (C) - Bedrock Core Taken (R) - Terminated at Refusal "NM" - Not Measured

THESE DRAWINGS SHALL NOT BE UTILIZED BY ANY PERSON, FIRM OR CORPORATION WITHOUT THE SPECIFIC WRITTEN PERMISSION OF FREEMAN COMPANIES, LLC

С

APPENDIX A

RECENT EXPLORATION LOGS

Page 10

The reported coordinates were acquired from consumer-grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

APPENDIX B

PREVIOUS TEST BORING LOGS

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APPENDIX C

RESULTS OF LABORATORY TESTING

Laboratory Measurement of Soil Resistivity Using the Wenner Four-Electrode Method by ASTM G57 (Laboratory Measurement)

Notes: Test Equipment: Nilsson Model 400 Soil Resistance Meter, MC Miller Soil Box Water added to sample to create a thick slurry prior to testing (saturated condition). Electrical Conductivity is calculated as inverse of Electrical Resistivity (per ASTM G57) Test conducted in standard laboratory atmosphere: 68-73 F

FUGRO CONSULTANTS, INC.

 PHONE (713) 369-5400 FAX (713) 369-5518

RESULTS OF TESTS

PROJECT: RECONSTRUCTOION OF EXIT CHARTER OAK BRIDGE (GTX 304831) REPORT DATE: 08-01-16 CLIENT NUMBER: JOB NUMBER: 04.1115-0003 FOR: GEOTESTING EXPRESS, INC. REPORT NUMBER: 125 NAGOG PARK ACTION, MA 01720 DATE SAMPLED: **TIME SAMPLED: REPORTED TO: ETHAN MARRO SAMPLED BY: CLIENT DATE RECEIVED: TIME RECEIVED:** SOLUBLE SULFATE AASHTO T-290 RECEIVED BY: SAMPLE ID | RESULTS | UNITS | LAB No. | TIME/DATE | ANALYST S1-S, S-2, 4 – 6' < 30 * mg/kg 0726052 1100/08-01-16 SD

Respectfully submitted,

**** WATER EXTRACTION PERFORMED BY USING A 1:10 RATIO OF SAMPLE AND REAGENT WATER FOLLOWED BY CENTRIFUGE AND VACUUME FILTRATION. THE WATER EXTRACT IS THEN ANALYZED USING THE ASTM D-512 AND D-516 METHODS.**

THE RESULTS RELATE AS TO THE LOCATION TESTED AND NO OTHER REFERENCE SHALL BE MADE. THIS REPORT SHALL NOT BE REPRODUCED EXCEPT IN FULL WITHOUT THE WRITTEN APPROVAL OF THE LABORATORY.

Steve DeGregorio Chemist

SD

*** Dry weight basis**

SO4CL 069-16

6100 HILLCROFT HOUSTON, TEXAS 77081

Bulk Density and Compressive Strength of Rock Core Specimens by ASTM D7012 Method C

Notes: Density determined on core samples by measuring dimensions and weight and then calculating.

All specimens tested at the approximate as-received moisture content and at standard laboratory temperature.

The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.

Failure Type: 1 = Intact Material Failure; 2 = Discontinuity Failure; 3 = Intact Material and Discontinuity Failure (See attached photographs)

- 1: Best effort end preparation. See Tolerance report for details.
- 2: The as-received core did not meet the ASTM side straightness tolerance due to irregularities in the sample as cored. 3: Specimen L/D < 2.
- 4: The as-received core did not meet the ASTM minimum diameter tolerance of 1.875 inches.
- 5: Specimen diameter is less than 10 times maximum particle size.
- 6: Specimen diameter is less than 6 times maximum particle size.

*Because the indicated tested specimens did not meet the ASTM D4543 standard tolerances, the results reported here may differ from those for a test specimen within tolerances.

UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO ASTM D4543

APPENDIX D

RESULTS OF L-PILE ANALYSES

9.625 m OID. CASING O.545 in TAARK NO ZE REBAR

FIXED HEAD 24 KIPS LATERAL 300KAS VERTICAL

9.625 in OD CASING TXED HEAD 15 KIPS LATERAL

9.625 in OD CASING
0.545 in Huck
No 28 Retar TKIPS LATERAL
300 KIPS VERTICAL

Lateral Deflection vs. Depth Deflection, in. 0.2 0.6 0.8 0.4 $\mathbf 0$ $\mathbf 0$ 5 10 15 20 Depth, feet
 $\frac{1}{2}$
 $\frac{30}{35}$ 40 45 50 55 60 **Loading Case 1** $\overline{\triangledown}$ LPile 2012.6.30, © 2012 by Ensoft, Inc.

LAND DEVELOPMENT | ENGINEERING DESIGN | CONSTRUCTION SERVICES

Geotechnical Report Rehabilitation of Bridge 05796 Route 15 NB over Silver Lane State Project No. 63-703 East Hartford, Connecticut

December 12, 2016

Freeman Project No.: 2014-1001

Prepared for: **CME Associates, Inc. 333 East River Drive, Suite 400 East Hartford, CT 06108**

Prepared by:

Freeman Companies, LLC 36 John Street Hartford, CT 06106

> Nathan L. Whetten, P.E., D.GE. Vice President of Geotechnical Services

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- B. Previous Test Boring Logs
- C. Results of Laboratory Testing

Geotechnical Report Rehabilitation of Bridge 05796 Route 15 NB over Main Street State Project No. 63-703 East Hartford, Connecticut December 12, 2016

1.0 INTRODUCTION

1.1 Summary

This report presents our evaluation of subsurface conditions and geotechnical engineering recommendations for rehabilitation of Bridge 05796, Route 15 over Silver Lane in East Hartford. Rehabilitation consists of widening the northbound (south) side of the bridge by 12 feet to accommodate an additional travel lane. The existing bridge is a single-span bridge supported on two full height abutments, which will be extended to the east. New U-type wingwalls will be provided.

We recommend that the widened portion of the abutments be supported on spread footings bearing on a layer of compacted granular fill placed over the native alluvial deposits. Bridge abutment loading will result in up to about 1.4 inches of settlement.

1.2 Scope of Work

Freeman Companies, LLC performed the following tasks:

- Engaged a subsurface exploration contractor to conduct test borings at the site.
- Provided technical monitoring of the explorations.
- Arranged for a testing laboratory to conduct laboratory soil tests.
- Evaluated the subsurface conditions.
- Conducted settlement evaluations.
- Prepared this report containing geotechnical design recommendations and construction considerations.

1.3 Authorization

The work was completed in accordance with our agreement dated October 21, 2015.

1.4 Project Vertical Datum

Elevations in this report are in feet and reference NAVD-88.

2.0 PROJECT AND SITE DESCRIPTION

2.1 Project Description

The bridge will be widened by 12 feet by extending Abutments 1 and 2 on the east side. New U-type wingwalls will be provided.

2.2 Site Description

The site is located on the south side of the Route 15 NB Bridge over Silver Lane, as shown on Figure 1, Site Location Map. The bridge is a single-span bridge supported on two full-height abutments. Silver Lane has two westbound travel

lanes and one eastbound lane, and sidewalks on each side. Ground surface south of the wingwalls consists of grass and shrubs.

Bridge grade is about El. 58 and Silver Lane grade below the bridge is about El. 33. The bridge abutments (existing and proposed) bear at El. 30; existing grade at the abutments is about El. 34.

3.0 EXPLORATIONS

3.1 Recent Explorations

Recent explorations included one Cone Penetrometer Test (CPT-5796-1) and one test boring (S-5796-1) conducted on June 14, 2016 and from May 9 to 13, 2016, respectively. The Cone Penetrometer Test (CPT) was conducted by ConeTec, of West Berlin, New Jersey, and the test boring was drilled by New England Boring Contractors, Inc., Glastonbury, Connecticut. CPT-5796-1 was located southeast of Abutment 1 and S-5796-1 was located southeast of Abutment 2.

CPT-5796-1 was drilled to a depth of 222.3 feet below ground surface using standard CPT push techniques, and the subsurface data was recorded continuously by a piezocone mounted on the tip. The CPT was terminated at the maximum push capacity of the rig, referred to on the log as "refusal". This refusal indicates that friction on the cone exceeded the capacity to push, and does not reflect the presence of a hard soil stratum.

Test boring S5796-1 was drilled to a depth of 319 feet below ground surface and was terminated at refusal. Standard Penetration Tests were conducted at maximum 5-foot-intervals and undisturbed tube samples of the lacustrine deposits were recovered from the boring. The completed borehole was backfilled with drill cuttings.

A Freeman Companies geologist monitored the drilling, described the soil samples, and prepared the test boring logs included in Appendix A, Recent Exploration Logs. The CPT log prepared by ConeTec is also included in Appendix A. Exploration locations were surveyed by CME Associates, and are shown on Figure 2, Subsurface Exploration Location Plan.

3.2 Previous Subsurface Explorations

Six previous test borings were drilled for the bridge, including B-10, and B-164 to B-168. Approximate locations of borings obtained from record documents are shown on Figure 2, Exploration Location Plan. Previous exploration logs and cross-sections of the previous explorations are provided in Appendix B.

3.3 Laboratory Testing

A laboratory testing program was conducted, consisting of:

- Eight moisture content tests,
- \bullet One grain size analysis,
- Two Constant Rate of Strain (CRS) Consolidation Tests,
- Four Atterberg Limit Determinations.

Geotechnical Report Rehabilitation of Bridge 05796 Route 15 NB over Main Street State Project No. 63-703 East Hartford, Connecticut December 12, 2016

Laboratory tests were conducted by Geotesting Express, of Acton, Massachusetts. Results of laboratory testing are provided in Appendix C, Laboratory Test Data. Results of previous and recent consolidation tests are plotted on Figure 3 Summary of Varved Clay Properties, East of Connecticut River.

4.0 SUBSURFACE CONDITIONS

4.1 Subsurface Conditions

Subsurface conditions encountered in the explorations include Fill, Alluvium, Lacustrine, and Glacial Till overlying Bedrock as described below. A summary of subsurface data is provided in Table I. A subsurface profile through Abutment 2 is provided on Figure 4.

Groundwater – Water was encountered in boring S5796-1 at a depth of 8 feet and in CPT5796-1 at a depth of 15 feet, corresponding to El. 28 and El. 21, respectively. However, these measurements were made during or shortly after drilling, and may not reflect stabilized groundwater. Groundwater levels will vary with season, water level in the nearby Connecticut River, precipitation, temperature, and other factors.

5.0 GEOTECHNICAL ENGINEERING RECOMMENDATIONS

5.1 Foundation Design Recommendations

Settlement - The proposed bridge widening will consist of extending the existing abutments, which are supported on spread footings. Settlement evaluations were conducted to determine the magnitude of anticipated settlement of the alluvial deposits and consolidation of the thick lacustrine deposits. The top of the lacustrine deposits is at approximately El. -24 (60 feet below ground surface), and the bottom is at El. -252 (288 feet below ground surface). Consolidation settlement is estimated to be about 1.4 inches in 50 years.

The compressible soils at a depth of 60 feet allows the consolidation settlement to be relatively uniform. Settlement will occur beneath both the new and existing portions of the bridge and approach embankments. Some of the settlement is ongoing settlement from the original construction.

This magnitude of settlement is more than the customary one inch of settlement commonly considered for design. However, we believe it is acceptable for this application. Other options to further mitigate settlement are either ineffective (e.g., use of lightweight fill does not significantly reduce settlement due to the depth of the clay), or too costly and difficult (e.g., pile foundations driven to refusal (319 feet in S5796-1)).

We recommend that the proposed abutments be supported on conventional spread footing foundations.

Foundation Design Criteria

- **Footings Foundation Depth:** Minimum of 4 feet below the lowest adjacent ground surface.
- **Seismic Design:** Soils are not susceptible to liquefaction. Soil conditions at the site are defined as AASHTO Site Class D.
- **Backfill Material:** Place Pervious Structure Backfill (CTDOT Form 817 M.02.05) behind the abutments and abutment wingwalls above a line defined by a 1V:1.5H slope extending up from the heel of the footing to grade.
- **Weep Holes:** 4 inch dia. weep holes at max 10 foot spacing, installed according to CTDOT specifications.
- **Lateral Earth Pressures:** Refer to Figure 5 Active Earth Pressures
- **Subgrade Preparation Below Abutments:** Minimum 12-inch thick layer of crushed stone (CTDOT Form 817 M.01.01 No. 6) overlying separation fabric (CTDOT Form 817 Sec. 7.55 M8.01-26) over the subgrade.
- **Service Limit Bearing:** 6,000 pounds per square foot (psf).
- **Strength Limit Bearing:** Nominal Bearing Resistance 20,000 psf, calculated using AASHTO Equation 10.6.3.1.3.
- **Settlement at Recommended Bearing Pressure:** Estimated total settlement approximately 1.4 inches; differential less than ¾- inch. Place a control joint at the connection between the existing and new portions of the abutments.
- **Coefficient of Friction (tan** δ **) Along Bottom:** 0.50 (AASHTO Table 3.11.5.3-1); Resistance factor 0.8 (AASHTO Table 10.5.5.2.2-1).
- **Global Stability:** We estimate a maximum resistance factor of 0.58 for the abutments for global stability (minimum factor of safety of 1.7). This is consistent with a load factor of 1.0 and a maximum resistance of 0.65 (AASHTO 11.6.2.3).

6.0 CONSTRUCTION CONSIDERATIONS

6.1 Excavation

Conventional excavation equipment appears practical for excavation. Excavation geometries should conform to OSHA excavation regulations contained in 29 CFR 1926, latest edition.

6.2 Abutment Bearing Surface Preparation

Excavated subgrades for the abutments should be covered with geotextile separation fabric and crushed stone placed over the fabric, and then proofrolled with a vibratory plate compactor. If the subgrade beneath the crushed stone is found to be excessively soft or yielding, it may be necessary to overexcavate the soft material and place additional crushed stone over fabric.

Geotechnical Report Rehabilitation of Bridge 05796 Route 15 NB over Main Street State Project No. 63-703 East Hartford, Connecticut December 12, 2016

Soil bearing surfaces should be protected against freezing both before and after concrete placement. If construction takes place during winter months, foundations should be backfilled as soon as possible following construction. Alternatively, insulating blankets or other methods may be used to protect against freezing.

6.3 Temporary Lateral Support

Temporary lateral support of excavations will be required to maintain and protect traffic flow and nearby utilities. Steel sheetpiling or soldier piles and lagging with multiple levels of bracing appears feasible. Surface water should be diverted away from excavations.

6.4 Excavation Dewatering

Excavation dewatering will be required to permit construction in-the-dry. Pumping from sumps located at the bottom of excavations appears feasible. Surface water should be diverted away from excavations. Pumping, handling, and treatment of excavation dewatering fluids should be in accordance with all applicable regulatory agency requirements.

6.5 Reuse of Existing Soils

The existing soils to be excavated will consist primarily of fill and silty sands with gravel. These soils are silty and are not expected to be suitable for reuse as Pervious Structure Backfill or Granular Fill. Excavated soils may be suitable for reuse as embankment fill. However the silty soils are difficult to properly compact when wet, and may need to be dried to achieve compaction. Drying the soils can be difficult and at times impractical, particularly during periods of cold and wet weather.

7.0 FUTURE SERVICES AND LIMITATIONS

We recommend that a qualified geotechnical engineer be engaged during construction to observe:

- Preparation of foundation bearing surfaces.
- Pile installation and load tests.
- Verify that soil conditions exposed in excavations are in general conformance with design assumption, and that the geotechnical aspects of construction are consistent with the project specifications.

This report was prepared for the exclusive use of CME Associates and the project design team. The recommendations provided herein are based on the project information provided at the time of this report and may require modification if there are any changes in the nature, design, or location of the structure.

The recommendations in this report are based in part on the data obtained from the subsurface explorations. The nature and extent of variations between explorations may not become evident until construction. If variations from the anticipated conditions are encountered, it may be necessary to revise the recommendations in this report.

Our professional services for this project have been performed in accordance with generally accepted engineering practices; no warranty, expressed or implied, is made.

2014-1001

Rehabilitation of Route 15 over Silver LaneContract CORE ID: 15DOT0148AA, State Project No. 63-703 East Hartford, Connecticut

Table 1

Subsurface Data

Notes:

1. Ground surface elevations at recent test borings were surveyed by CME Associates, Inc. Ground surface elevation at previous borings were shown on the logs and corrected to NAVD-88 on this table.

2. Groundwater levels are approximate.

3. ">" - Greater Than "--" - Not Encountered (C) - Bedrock Core Taken (R) - Terminated at Refusal "NM" - Not Measured

FIGURES

THESE DRAWINGS SHALL NOT BE UTILIZED BY ANY PERSON, FIRM OR CORPORATION WITHOUT THE SPECIFIC WRITTEN PERMISSION OF FREEMAN COMPANIES, LLC

NOTES

1. PREVIOUS DATA WAS OBTAINED FROM THE RECORD REPORT TITLED "GEOTECHNICAL LABORATORY DATA REPORT, CHARTER OAK BRIDGE AND APPROACHES, HARTFORD-EAST HARTFORD,

CONNECTICUT" DATED MAY 1987.

- 2. ELEVATIONS REFER TO NAVD-88. PREVIOUS ELEVATIONS WERE ADJUSTED FROM NGVD-29.
- **DEFINITIONS**
- COMPRESSION RATIO $(=\Delta \varepsilon/\Delta \log \sigma'_{V})$ DURING VIRGIN COMPRESSION **CR** $\qquad \qquad -$
- RECOMPRESSION RATIO $(=\Delta \varepsilon / LOG\sigma'_{V})$ during recompression **RR** $\overline{}$
- $\sigma'{}_{\mathsf{V}\mathsf{O}}$ IN SITU VERTICAL EFFECTIVE STRESS $\overline{}$
- PRECONSOLIDATION STRESS σ_P –

SUMMARY OF VARVED CLAY PROPERTIES **EAST OF CONNECTICUT RIVER** STATE PROJECT NO. 63-703 HARTFORD, CONNECTICUT **FIGURE 3B**

Freeman Companies, LLC

36 John StreetHartford, CT 06109

TKT).GP. STRATIGRAPHY & GW - A SIZE - GINT STD US.GDT - 10/21/16 15:07 - Y:\2014\2014-1001 CONNDOT CSO 2232 CME\GEOT\GINT\2014-1001 - CHARTER OAK BRIDGE LOGS (TKT).GPJ CME\GEOT\GINT\2014-1001 - CHARTER OAK BRIDGE LOGS (2232 **CSC** STRATIGRAPHY & GW - A SIZE - GINT STD US.GDT - 10/21/16 15:07 - Y:2014/2014-1001 CONNDOT

С

APPENDIX A

RECENT EXPLORATION LOGS

The reported coordinates were acquired from consumer-grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

APPENDIX B

PREVIOUS TEST BORING LOGS

502

THIS SHEET NC

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THE INFORMATION, INCLUDING ESTIMATED QUANTITIES OF WORK SHOWN ON THESE SHEETS IS BASED ON LIMITED INVES-TIGATIONS BY THE STATE AND IS IN NO WAY WARRANTED TO INDICATE THE TRUE CONDITIONS OR ACTUAL QUANTITIES OR DISTRIBUTION OF QUANTITIES OF WORK WHICH WILL BE REQUIRED.

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42-225

THE INFORMATION, INCLUDING ESTIMATED QUANTITIES OF WORK SHOWN ON THESE SHEETS IS BASED ON LIMITED INVES-TIGATIONS BY THE STATE AND IS IN NO WAY WARRANTED TO INDICATE THE TRUE CONDITIONS OR ACTUAL QUANTITIES OR DISTRIBUTION OF QUANTITIES OF WORK WHICH WILL BE REQUIRED.

APPENDIX C

RESULTS OF LABORATORY TESTING

Moisture Content of Soil and Rock - AASHTO T 265

Moisture Content of Soil and Rock - AASHTO T 265

AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample/Test Description Sand/Gravel Particle Shape : ANGULAR Sand/Gravel Hardness : HARD

#60 #100 #200

0.25 0.15 0.075 23 16 11

Sample Prepared using the WET method

Dry Strength: MEDIUM Dilatancy: RAPID Toughness: MEDIUM

Sample Prepared using the WET method

Dry Strength: HIGH Dilatancy: NONE Toughness: MEDIUM

Sample Prepared using the WET method

Dry Strength: HIGH Dilatancy: SLOW Toughness: MEDIUM

Sample Prepared using the WET method

Dry Strength: MEDIUM Dilatancy: NONE Toughness: MEDIUM

Constant Rate of Consolidation

Constant Strain Rate by ASTM D4186

Constant Rate of Consolidation Constant Strain Rate by ASTM D4186 Pressure Curves

CRC TEST DATA

Note: Specific Gravity and Void Ratios are calculated assuming the degree of saturation equals 100% at the end of the test. Therefore, values may not represent actual values for the specimen.

Constant Rate of Consolidation

Constant Strain Rate by ASTM D4186 Summary Report

Constant Rate of Consolidation Constant Strain Rate by ASTM D4186 Pressure Curves

CRC TEST DATA

Note: Specific Gravity and Void Ratios are calculated assuming the degree of saturation equals 100% at the end of the test. Therefore, values may not represent actual values for the specimen.

LAND DEVELOPMENT | ENGINEERING DESIGN | CONSTRUCTION SERVICES

Geotechnical Report Rehabilitation of Bridge 06000A Route 5/15 NB over I-91 NB, Reserve Road, Route 2, CT River and Railroad State Project No. 63-703 Hartford and East Hartford, Connecticut

February 14, 2017

Freeman Project No.: 2014-1001

Prepared for: **CME Associates, Inc. 333 East River Drive, Suite 400 East Hartford, CT 06108**

Prepared by:

Freeman Companies, LLC 36 John Street Hartford, CT 06106

> Nathan L. Whetten, P.E., D.GE. Vice President of Geotechnical Services

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1. Summary of Subsurface Data

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- 1. Site Location Map
- 2. Subsurface Exploration Location Plan
- 3. Summary of Varved Clay Properties, West of Connecticut River
- 4. Subsurface Profiles
- 5. Lateral Earth Pressures Active

Appendices

- A. Recent Test Boring Logs
- B. Previous Test Boring Logs
- C. Results of Laboratory Testing
- D. Draft Special Provisions

1.0 INTRODUCTION

1.1 Summary

This report presents our evaluation of subsurface conditions and geotechnical engineering recommendations for rehabilitation of Bridge 06000A, Route 5/15 NB over I-91 NB, Reserve Road, Route 2, CT River, and Railroad. Abutment 1 and Piers 1, 2, and 3 will be widened to accommodate two additional travel lanes.

We recommend that the widened abutments and piers be supported on steel H-Piles driven to refusal on bedrock, and pile tip reinforcement should be provided. Filling behind the Abutment 1 and wingwall will result in settlement of subgrade soils and downdrag loads on abutment piles will occur. Additionally, soils at Abutment 1 and at the piers were found to be corrosive. We recommend that bitumen coatings be applied to piles supporting Abutment 1 and the piers to provide protection against corrosion, and to reduce downdrag at Abutment 1. Preaugering will be required to protect the coatings.

1.2 Scope of Work

Freeman Companies, LLC performed the following tasks:

- Engaged a subsurface exploration contractor to conduct test borings at the site.
- Provided technical monitoring of the explorations.
- Arranged for a testing laboratory to conduct laboratory soil tests.
- Evaluated the subsurface conditions
- Conducted settlement evaluations
- Prepared this report containing geotechnical design recommendations and construction considerations.

1.3 Authorization

The work was completed in accordance with our agreement dated October 21, 2015.

1.4 Project Vertical Datum

Elevations in this report are in feet and reference NAVD-88.

2.0 PROJECT AND SITE DESCRIPTION

2.1 Project Description

Abutment 1 will be widened by 33 feet on the east side, and Piers 1, 2, and 3 will be widened by an average of about 21 feet to accommodate the additional travel lanes. The pile cap supporting Abutment 1 will be enlarged to support the widened abutment. The widened portions of Piers 1, 2, and 3 will be supported on new pile cap foundations constructed adjacent to the existing foundations.

2.2 Site Description

Abutment 1 will be widened on the southeast side, between the existing abutment and the on-ramp from Route 5/15 to I-91 NB. The area slopes downward to the southeast to the on-ramp, and is grass-covered with some trees. Ground surface is about El. 67 at bridge grade, and slopes from approximately El. 46 to 34 in the area of the abutment widening.

Piers 1 and 2 are located north of I-91 NB and south of Reserve Road and railroad tracks. Pier 3 is located north of Reserve Road. Ground surface is gravel covered and at about El. 48 at Pier 1, El. 36 at Pier 2, and El. 35 at Pier 3.

3.0 EXPLORATIONS

3.1 Recent Explorations

Four test borings (S2-1 through S2-4) were drilled by New England Boring Contractors, Inc., Glastonbury, Connecticut. Boring S2-1 was drilled Abutment 1, and borings S2-2, S2-3, and S2-4 were drilled near Piers 1, 2, and 3. Borings were drilled to depths ranging from 64 to 100 feet below ground surface. Standard Penetration Tests were completed at maximum 5 foot intervals within the test borings. Ten-foot-long NX-size rock cores were obtained from each boring. Explorations were backfilled with drill cuttings. A groundwater monitoring well was installed in boring S2-3 OW to measure groundwater levels. A roadway box was placed at ground surface to protect the installation.

A Freeman Companies geologist monitored the drilling, described the soil samples, and prepared the test boring logs included in Appendix A, Recent Boring Logs. Exploration locations were surveyed by CME Associates, and are shown on Figure 2, Subsurface Exploration Location Plan.

3.2 Previous Subsurface Explorations

Several previous test borings were drilled in the vicinity of the new bridge and are considered applicable, including B-103, B-104, B-107, B-109, B-111, B-114, and B117A. Approximate locations of borings obtained from record documents are shown on Figure 2, Exploration Location Plan, and logs are provided in Appendix B.

3.3 Laboratory Testing

A laboratory testing program was conducted, consisting of:

- Twelve moisture content tests
- Two pH tests, two electrical resistivity tests, and two soluble sulfate tests
- \bullet Five grain size analyses
- Three Constant Rate of Strain (CRS) Consolidation Tests
- Six Atterberg Limit Determinations
- One unconfined compression test on a rock core sample.

Laboratory tests were conducted by Geotesting Express, of Acton, Massachusetts. Results of laboratory testing are provided in Appendix C, Laboratory Test Data. Results of previous and recent consolidation tests are plotted on Figure 3 Summary of Varved Clay Properties, West of Connecticut River.

4.0 SUBSURFACE CONDITIONS

4.1 Subsurface Conditions

Subsurface conditions encountered in the explorations include Fill, Alluvium, Lacustrine, and Glacial Till overlying Bedrock as described below. A summary of subsurface data is provided in Table I. Subsurface profiles at the abutments and piers are provided on Figures 4A through 4D, Subsurface Profiles.

Groundwater – Water was encountered in the borings at depths ranging from 6 to 18 feet (El 4 to El 18). Groundwater was measured in the observation well S2-3 (OW) at El. 7.6, nine months after the well was installed. Groundwater levels were measured during drilling activities and may not represent static levels, except at observation wells. Water levels will vary with season, water level in the nearby Connecticut River, precipitation, temperature, and other factors.

Corrosion – Corrosion testing was conducted on samples recovered from test borings S1-2 (Abutment 1), S1-5 (Pier 2), and S1-12 (Abutment 2). Results are summarized below:

5.0 GEOTECHNICAL ENGINEERING RECOMMENDATIONS

5.1 Foundation Design Recommendations

Downdrag – The threshold settlement for downdrag loads on piles is commonly considered to be 0.4 inches. Settlement evaluations were conducted at the proposed abutments to estimate the magnitude of total settlement, and whether settlement would cause downdrag at the existing and proposed piles. Predicted total settlement calculated using the computer program Settle 3D (by RocScience) is as follows:

Normal Weight Fill: 2¹/₂ inches south of abutment; 1¹/₄ inches at abutment (incl. ¹/₂ inch on-going secondary) Expanded Shale: 1½ inches south of the abutment; 1 inch at the abutment (incl. ½ inch secondary) Geofoam: 3/4 inch south of the abutment; $\frac{1}{2}$ inch at the abutment (incl. 0.4 inch secondary)

These settlements will result in downdrag loads on the abutment piles. We recommend that coatings be applied to piles to reduce downdrag loads at the abutments, or that piles be oversized to allow for downdrag. A 90 percent reduction in downdrag loads is considered feasible using bitumen coatings, whereas a 33 percent reduction in downdrag has been reported for an epoxy coating referred to as *Slickcoat*. We recommend that bitumen coatings be considered for this project. We recommend that backfill consist of expanded shale aggregate.

Corrosion – AASHTO Section 10.7.5 indicates that soils are corrosive if pH is less than 5.5, resistivity is less than 2,000 ohm-cm, or sulfate concentration is greater than 1,000 ppm. Based on these criteria, soils at the Abutment 1 and the piers are considered corrosive. Corrosion mitigation methods typically include providing a protective coating (AASHTO C10.7.5). The NCHRP report titled *"Design and Construction Guidelines for Downdrag on Uncoated and Bitumen Coated Piles",* Briaud and Tucker, 1996, pg. 10, indicates that bitumen coatings provide corrosion resistance.

We recommend that bitumen coatings be applied to piles at Abutment 1, to provide both corrosion protection and downdrag mitigation. Bitumen coating should also be applied to piles at the piers to provide corrosion resistance. Alternatively, epoxy-coated piles may be considered for corrosion protection at the piers.

Pile Design

- **Seismic Design:** Soils are not susceptible to liquefaction. Soil conditions at the site are defined as AASHTO Site Class E. Assume peak ground acceleration (PGA) of 0.061g, a short-term acceleration coefficient $S_{s}=$ 0.132g and long-term acceleration coefficient $S_1 = 0.037g$, respectively.
- **Pile Type:** HP12x74 with pile tip reinforcement driven to end bearing on bedrock, Grade 50 steel. Other H-Pile sections may also be considered.
- **Service Limit:** 125 tons, assumes a HP12x74 pile area equal to 21.76 square inches. Subtract an appropriate allowance for downdrag for piles supporting the abutments, as indicated below.
- **Strength Limit:** For end bearing piles, assume a strength limit equal to the structural capacity of the pile. Settlement of piles is expected to be equal to the elastic compression of the pile.

• **Downdrag:** Estimated downdrag loads are listed below:

Abutment 1:

160 tons (single piles, uncoated) or 16 tons (single pile with bitumen coating)

14.5 tons (corner pile in a group with bitumen coating)

13 tons (side pile in a group with bitumen coating)

8 tons (inside pile in a group with bitumen coating)

- **Load Tests:** Minimum of 3 dynamic load tests with matching signal analysis (4 tests if 26 or more piles, and no less than 2% of the production piles, AASHTO Table 10.5.5.2.3-3).
- **Test Piles:** Recommend same piles and criteria as load tests (AASHTO 10.7.9)
- **Minimum Spacing:** Center to center spacing should be 2½ times the pile diameter (AASHTO 2012 10.7.1.2) and at least 30 inches. Minimum 9 inches to the nearest edge of the pile cap
- **Lateral Resistance:** Use the pile capacity in batter. Additional lateral load capacities in bending will be provided based on LPile analyses once pile loading is established.
- **Subgrade Preparation Below Pile Cap:** Pile cap subgrades are expected to occur within silty soils that can easily be disturbed and become unstable. We recommend a minimum 12-inch thick layer of crushed stone (CTDOT Form 817 M.01.01 No. 6) overlying separation fabric (CTDOT Form 817 Sec. 7.55 M8.01-26) over the subgrade.

• **Bottom of Structure and Estimated Pile Length:**

Substructure	Bottom of Pile Cap Elevation	Estimated Pile Tip Elevation
Abutment 1	26.1	-61
Pier 1	9.5	-62
Pier 2	15.8 (west support) 14 (east	-56
	support)	
Pier 3	20	-51

Abutment Design

6.0 CONSTRUCTION CONSIDERATIONS

6.1 Excavation

Proposed bottom of pile caps will be within the Fill and Alluvium strata. The alluvium and portions of the fill are highly susceptible to disturbance by construction equipment, and are expected to be wet due to shallow groundwater. Excavation to footing subgrade should be made using a smooth-bladed backhoe bucket. Excavation geometries should conform to OSHA excavation regulations contained in 29 CFR 1926, latest edition.

6.2 Pile Cap Subgrade Preparation

The alluvium and portions of the fill have low strength and are highly susceptible to disturbance from construction equipment and vibrations. The contractor shall anticipate that a temporary working pad will be necessary to support installation equipment. We anticipate that working pads could potentially include multiple layers of geogrids, stabilization fabric, crushed stone, well-graded sand and gravel aggregate, or other materials, and the working pad may need to be on the order of three feet thick. The contractor shall be responsible for design of an appropriate working pad capable of supporting his proposed installation equipment. A draft special provision is provided in Appendix D.

Soil bearing surfaces should be protected against freezing both before and after concrete placement. If construction takes place during winter months, foundations should be backfilled as soon as possible following construction. Alternatively, insulating blankets or other methods may be used to protect against freezing.

6.3 Pile Installation

The maximum hammer energy should be determined by a wave equation analysis by the contractor based on the specific hammer characteristics. Test piles and dynamic load testing should be conducted as indicated above. Vibrations from pile driving should not affect the structural integrity of adjacent structures. However, vibration and noise will likely be noticeable inside buildings 300 feet away, or more.

Coatings should be applied to the piles prior to transportation to the site. It should include a primer coat that may be sprayed or painted onto the piles, and a final coat.

Piles with bitumen or epoxy coatings should be installed in a preaugered and cased hole to avoid damage to the piles during pile driving. Piles should be preaugered through the existing fill and alluvial deposits (granular soils) to the top of lacustrine deposits. Additionally, the alluvium is expected to be susceptible to settlement from pile driving, and settlement of the alluvial deposits could affect nearby structures and utilities. The top of lacustrine deposits is typically about El -20. Sand should be placed in the casing as the casing is extracted.

Draft special provisions are provided in Appendix D.

6.4 Expanded Shale Aggregate

Expanded shale aggregate should be placed in layers 1.5 to 2 feet thick, and compacted with self-propelled vibratory compaction equipment with static weight less than 6,600 lbs. The minimum number of passes should be limited to two and the maximum four, to avoid particle breakdown during compaction. A draft special provision is included in Appendix D.

6.5 Temporary Lateral Support

We estimate that excavations will be required to reach the pile cap subgrade. Temporary lateral support of excavations will be required to maintain and protect traffic flow, and to protect nearby utilities. Steel sheetpiling or soldier piles and lagging with multiple levels of bracing appears feasible. Surface water should be diverted away from excavations.

6.6 Excavation Dewatering

Excavation dewatering will be required to permit construction in in-the-dry. Pumping from sumps located in the bottom of excavations appears feasible. Surface water should be diverted away from excavations. Pumping, handling, and treatment of excavation dewatering fluids should be in accordance with all applicable regulatory agency requirements.

6.7 Reuse of Existing Soils

The existing soils to be excavated will consist primarily of fill and silty sands with gravel. These soils are silty and are not expected to be suitable for reuse as Pervious Structure Backfill or Granular Fill. Excavated soils may be suitable for reuse as embankment fill. However the silty soils are difficult to properly compact when wet, and may need to be dried to achieve compaction. Drying the soils can be difficult and at times impractical, particularly during periods of cold and wet weather.

7.0 FUTURE SERVICES AND LIMITATIONS

We recommend that a qualified geotechnical engineer be engaged during construction to observe:

- Preparation of foundation bearing surfaces
- Pile installation and load tests
- Verify that soil conditions exposed in excavations are in general conformance with design assumption, and that the geotechnical aspects of construction are consistent with the project specifications.

This report was prepared for the exclusive use of CME Associates and the project design team. The recommendations provided herein are based on the project information provided at the time of this report and may require modification if there are any changes in the nature, design, or location of the structure.

The recommendations in this report are based in part on the data obtained from the subsurface explorations. The nature and extent of variations between explorations may not become evident until construction. If variations from the anticipated conditions are encountered, it may be necessary to revise the recommendations in this report.

Our professional services for this project have been performed in accordance with generally accepted engineering practices; no warranty, express or implied, is made.

2014-1001Bridge 06000A Rt 15 SB over I-91 NB Rt. 2 & CT River & RR Contract CORE ID: 15DOT0148AA, State Project No. 63-703 Hartford, Connecticut

Table 1

Notes:

1. Ground surface elevations at recent test borings were surveyed by CME Associates, Inc. Ground surface elevations at previous borings were shown on the logs and corrected to NAVD-88 in this table.

2. Groundwater levels are approximate

3. Top of bedrock is inclusive of weathered rock

4. ">" - Greater Than "--" - Not Encountered (C) - Bedrock Core Taken "NM" - Not Measured

FIGURES

THESE DRAWINGS SHALL NOT BE UTILIZED BY ANY PERSON, FIRM OR CORPORATION WITHOUT THE SPECIFIC WRITTEN PERMISSION OF FREEMAN COMPANIES, LLC

NOTES

 $1.$

PREVIOUS DATA WAS OBTAINED FROM THE REPORT TITLED

BRIDGE AND APPROACHES, HARTFORD-EAST HARTFORD,

CONNECTICUT" DATED MAY 1987.

ADJUSTED FROM NGVD-29.

"GEOTECHNICAL LABORATORY DATA REPORT, CHARTER OAK

2. ELEVATIONS REFER TO NAVD-88. PREVIOUS ELEVATIONS WERE

- **DEFINITIONS**
- COMPRESSION RATIO (= $\Delta \varepsilon / \Delta \text{LOG} \sigma'_{V}$) DURING VIRGIN COMPRESSION **CR** $\overline{}$
	- RECOMPRESSION RATIO (= Ae/LOGo'v) DURING RECOMPRESSION **RR**
	- IN SITU VERTICAL EFFECTIVE STRESS σ'νο
	- PRECONSOLIDATION STRESS σ_P $\overline{}$

SUMMARY OF VARVED CLAY PROPERTIES WEST OF CONNECTICUT RIVER STATE PROJECT NO. 63-703 HARTFORD, CONNECTICUT **FIGURE 3A**

Freeman Companies, LLC

36 John Street

SUBSURFACE DIAGRAM

SUBSURFACE DIAGRAM

Freeman Companies, LLC

SUBSURFACE DIAGRAM

Freeman Companies, LLC

SUBSURFACE DIAGRAM

ACTIVE EARTH PRESSURESREHABILITATION OF BRIDGE 06000ASTATE PROJECT NO. 63-703HARTFORD, CONNECTICUT

CHECKED: APPROVED: SCALED: PROJECT NO.: DATE: FIG.

FIGURE 5

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LAND DEVELO

36 JOHN STREET HARTFORD, CT 06106 WWW.FREEMANCOS.COMTEL:(860)251-9550 FAX:(860)986-7161 ELEVATE YOUR EXPECTATIONS

ENGINEERING DESIGN I CONSTRUCTION SERVICE

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APPENDIX A

RECENT TEST BORING LOGS

APPENDIX B

PREVIOUS TEST BORING LOGS

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APPENDIX C

RESULTS OF LABORATORY TESTING

Moisture Content of Soil and Rock - AASHTO T 265

Notes: Temperature of Drying : 110º Celsius

Moisture Content of Soil and Rock - AASHTO T 265

Notes: Temperature of Drying : 110º Celsius

pH of Soil by ASTM D4972

Notes: Sample Preparation: screened through #10 sieve Method A, pH meter used

Laboratory Measurement of Soil Resistivity Using the Wenner Four-Electrode Method by ASTM G57 (Laboratory Measurement)

Notes: Test Equipment: Nilsson Model 400 Soil Resistance Meter, MC Miller Soil Box Water added to sample to create a thick slurry prior to testing (saturated condition). Electrical Conductivity is calculated as inverse of Electrical Resistivity (per ASTM G57) Test conducted in standard laboratory atmosphere: 68-73 F

FUGRO CONSULTANTS, INC.

PROJECT: RECONSTRUCTOION OF EXIT CHARTER OAK BRIDGE

 PHONE (713) 369-5400 FAX (713) 369-5518

**** WATER EXTRACTION PERFORMED BY USING A 1:10 RATIO OF SAMPLE AND REAGENT WATER FOLLOWED BY CENTRIFUGE AND**

VACUUME FILTRATION. THE WATER EXTRACT IS THEN ANALYZED USING THE ASTM D-512 AND D-516 METHODS. THE RESULTS RELATE AS TO THE LOCATION TESTED AND NO OTHER REFERENCE SHALL BE MADE.

THIS REPORT SHALL NOT BE REPRODUCED EXCEPT IN FULL WITHOUT THE WRITTEN APPROVAL OF THE LABORATORY.

RESULTS OF TESTS

 (GTX 304831) CLIENT NUMBER: JOB NUMBER: 04.1115-0003 FOR: GEOTESTING EXPRESS, INC. REPORT NUMBER: 125 NAGOG PARK ACTION, MA 01720 TIME SAMPLED: REPORTED TO: ETHAN MARRO SAMPLED BY: CLIENT DATE RECEIVED: TIME RECEIVED: SOLUBLE SULFATE AASHTO T-290 RECEIVED BY: SAMPLE ID | RESULTS | UNITS | LAB No. | TIME/DATE | ANALYST S1-S, S-2, 4 – 6' < 30 * mg/kg 0726052 1100/08-01-16 SD S1-5, S-3, 10 – 12' | 57 * | mg/kg | 0726053 | 1100/08-01-16 | SD S1-12, S-2, 5 – 7' \vert \vert \vert \vert \vert \vert \vert 50 \vert \vert mg/kg \vert 0726054 | 1100/08-01-16 | SD S2-1, S-4, 15 – 17' | < 50 * | mg/kg | 0726055 | 1100/08-01-16 | SD S2-3, S-2, 5 – 7' | 297 * | mg/kg | 0726056 | 1100/08-01-16 | SD S-0480-1, S-5, 14 – 16' | 543 * | mg/kg | 0726057 | 1100/08-01-16 | SD

6100 HILLCROFT HOUSTON, TEXAS 77081

REPORT DATE: 08-01-16

SO4CL 069-16

S-0480-2, S-3, 9 – 11' 355 * mg/kg 0726058 1100/08-01-16 SD S-06043-41, S-2, 5 – 7' < 30* mg/kg 0726059 1100/08-01-16 SD

Steve DeGregorio Chemist

Respectfully submitted,

SD

 *** Dry weight basis**

Sample Comment: ---

ASTM N/A

AASHTO Silty Soils (A-4 (0))

Sample/Test Description Sand/Gravel Particle Shape : ---

Sand/Gravel Hardness : ---

Sample Comment: ---

AASHTO Silty Soils (A-4 (0))

Sample/Test Description Sand/Gravel Particle Shape : ---

Sand/Gravel Hardness : ---

AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample/Test Description Sand/Gravel Particle Shape : ANGULAR Sand/Gravel Hardness : HARD

 $#100$ #200

 0.15 0.075 $\overline{10}$ 12

Atterberg Limits - AASHTO T 89 and T 90

Sample Prepared using the WET method

Dry Strength: VERY HIGH Dilatancy: SLOW Toughness: LOW

Atterberg Limits - AASHTO T 89 and T 90

Sample Prepared using the WET method

Dry Strength: VERY HIGH Dilatancy: SLOW Toughness: LOW

Atterberg Limits - AASHTO T 89 and T 90

Sample Prepared using the WET method

Atterberg Limits - AASHTO T 89 and T 90

Sample Prepared using the WET method

Atterberg Limits - AASHTO T 89 and T 90

Sample Prepared using the WET method

Sample Comment: ---

Atterberg Limits - AASHTO T 89 and T 90

Sample Prepared using the WET method

Constant Rate of Consolidation

Constant Strain Rate by ASTM D4186 Summary Report

Constant Rate of Consolidation Constant Strain Rate by ASTM D4186

Pressure Curves

CRC TEST DATA

Soil Description: Moist, dark reddish brown clay Remarks: System Y

Note: Specific Gravity and Void Ratios are calculated assuming the degree of saturation equals 100% at the end of the test. Therefore, values may not represent actual values for the specimen.

Constant Rate of Consolidation

Constant Strain Rate by ASTM D4186 Summary Report

 \circ $\overline{5}$ Strain, $\frac{8}{0}$ 15 $20 -$ 100 1000 10000 100000 10^{-2} 10^{-3} Cv , ft^o 2 /sec 10^{-4} 10^{-5} 10^{-6} $10^{-7} -$ 100 1000 100000 10000 Effective Stress, psf

Constant Rate of Consolidation Constant Strain Rate by ASTM D4186

Pressure Curves

CRC TEST DATA

Soil Description: Moist, dark reddish brown clay Remarks: System O

Note: Specific Gravity and Void Ratios are calculated assuming the degree of saturation equals 100% at the end of the test. Therefore, values may not represent actual values for the specimen.

Constant Rate of Consolidation

Constant Strain Rate by ASTM D4186 Summary Report

Constant Rate of Consolidation Constant Strain Rate by ASTM D4186 Pressure Curves

3000 2000 psf 1000 Excess Pressure, \circ -1000 -2000 $-3000 -$ 100000 1000 100 10000 0.6 0.4 0.2 Pressure Ratio 0.0 -0.2 -0.4 $-0.6 -$ 1000 100000 100 10000 Effective Stress, psf

Note: Specific Gravity and Void Ratios are calculated assuming the degree of saturation equals 100% at the end of the test. Therefore, values may not represent actual values for the specimen.

Bulk Density and Compressive Strength of Rock Core Specimens by ASTM D7012 Method C

Notes: Density determined on core samples by measuring dimensions and weight and then calculating.

All specimens tested at the approximate as-received moisture content and at standard laboratory temperature.

The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.

Failure Type: 1 = Intact Material Failure; 2 = Discontinuity Failure; 3 = Intact Material and Discontinuity Failure (See attached photographs)

- 1: Best effort end preparation. See Tolerance report for details.
- 2: The as-received core did not meet the ASTM side straightness tolerance due to irregularities in the sample as cored. 3: Specimen L/D < 2.
- 4: The as-received core did not meet the ASTM minimum diameter tolerance of 1.875 inches.
- 5: Specimen diameter is less than 10 times maximum particle size.
- 6: Specimen diameter is less than 6 times maximum particle size.

*Because the indicated tested specimens did not meet the ASTM D4543 standard tolerances, the results reported here may differ from those for a test specimen within tolerances.

UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

APPENDIX D

DRAFT SPECIAL PROVISIONS

ITEM #0203xxxA – EQUIPMENT WORKING PAD

Description:

Form 817, Section 203, Structure Excavation shall apply with the following amendments:

Article 2.03.03 – Construction Methods: Insert the following provisions at the end of Item 2, Preparation of Foundations:

The alluvium and portions of the fill have low strength and are highly susceptible to disturbance from construction equipment and vibrations. The contractor shall anticipate that a temporary working pad will be necessary to support installation equipment. Working pads could potentially include multiple layers of geogrids, stabilization fabric, crushed stone, well-graded sand and gravel aggregate, or other materials, and the working pad may need to be on the order of three feet thick. The contractor shall be responsible for design of an appropriate working pad capable of supporting his proposed installation equipment.

ITEM #0702081A- BITUMINOUS COATING FOR STEELPILES

Description: Work under this item shall consist of furnishing and applying bituminous coating to steel piles. This work shall be performed as hereinafter specified, to the dimensions indicated on the plans, or as directed by the Engineer. This work shall also include field applied touch ups to coating damaged during shipping and handling.

Materials: Provide bituminous coating for all piles. Bituminous coating shall consist of canal liner bituminous in accordance with ASTM D 2521. It shall have a softening point of 190°F to 200°F a penetration of 56 to 61 at 77°F and a ductility in excess of 1.38 in. at 77°F. Primer shall be in accordance with AASHTO M 116.

Construction Methods:

- A. All surfaces to be coated with bituminous shall be dry and thoroughly cleaned of dust and loosematerials.
- B. Primer or bituminous shall not be applied in wet weather, nor when the ambient temperature is below 65°F.
- C. Application of the prime coat shall be with a brush or other approved means and in a manner which thoroughly coats the surface of the piling with a continuous film of primer. The primer shall have set thoroughly before the bituminous coating is applied. The bituminous shall be heated to 300°F and applied at a temperature between 200° and 300°F by means of one or more mop coats or other approved means.
- D. The average coating thickness shall be 1/16".
- E. Whitewashing of the coating may be required during hot weather as directed to prevent running or sagging of the asphalt coating prior to driving of the pile.
- F. Bituminous coated piles shall be protected from sunlight or heat immediately after the coating is applied.
- G. The bituminous coating shall not be exposed to damage or contamination during storage, hauling, or handling. Once the bituminous coating has been applied, dragging the piles on the ground or the use of cable wraps around the piles during handling will not be permitted. Pad eyes, or other suitable devices, shall be attached to the piles to be used for lifting and handling.
- H. Where Field splices are required the bituminous coating shall be removed in the splice area. After completing the field splice, the splice area shall be brush coated or mop coated with a minimum of one coat of bituminous material as directed.

Method of Measurement: Bituminous coating will be measured per linear foot of pile coated.

Basis of Payment: Payment shall be made at the contract unit price per linear foot of pile coated. This price shall be full compensation for furnishing all materials, for preparing and placing these materials, and for all labor, equipment tools, and incidentals necessary to complete

ITEM #0702081A

ITEM #0702109A- PRE-AUGERING OF PILES

ITEM #0702111A- DRIVING STEEL PILES

Work under this item shall conform to the requirements of Section 7.02 of Form 817 as replaced by the special provision for Section 7.02 in this contract, amended as follows:

7.02.01- Description: Add the following:

Work under this Item includes pre-augering for piles as indicated on the Plans or as ordered by the Engineer.

7.02.03.2(a) - Construction Methods - Pile Driving Equipment - Hammers: Replace the second paragraph with the following:

The size of hammer shall be adapted to the type and size of piles and the driving conditions. Unless otherwise specified, the minimum rated striking energy per blow for hammers used shall be 26,000-foot pounds (35,000 joules) for driving steel piles. The hammer model used for the driving of test piles shall be used for the driving of service or production piles, unless a change is authorized by the Engineer in writing. Hammers delivering an energy which the Engineer considers detrimental to the piles shall not be used.

7.02.03.2(7) - Construction Methods - Pile Driving Equipment - Pre-Augering: Add the following:

The following apply when pre-auguring is done for piles with bituminous and epoxy coating:

The pre-augered hole is to continue to the top of the clay layer or to the depths shown on the plans or as directed by the Engineer. The pre-augered hole diameter shall be at least the diagonal dimension of the pile, or as directed by the Engineer. All obstructions which could interfere with the driving of piles within the depth of pre-augering are to be removed as part of the pre-auguring work.

The Contractor shall provide temporary casing to maintain the pre-augured dimension of the hole. Upon completion of pile driving, the annulus between the pile and outer hole diameter shall be filled with clean sand and any temporary casing will be removed.

7.02.05.11 - Basis of Payment - Pre-Augering of Piles: Add the following:

This work shall also include obstruction removal, casing, and sand backfill

ITEM #0207150A - LIGHTWEIGHT FILL

Description: Work shall consist of furnishing and placing lightweight fill in the formation of embankments or as backfill in front of and behind structures. This work shall be performed as hereinafter specified, to the dimensions indicated on the plans, or as directed by the Engineer. This item shall also consist of furnishing and placing crushed stone or gravel in burlap bags at the inlet ends of weep holes in structures to the dimensions indicated on the plans or as ordered by the Engineer.

Materials: Lightweight fill shall be a rotary kiln expanded shale aggregate meeting the requirements of ASTM C 330. No by-product slags, cinders or by-products of coal combustion shall be permitted. The aggregate shall consist of tough, durable, non-corrosive particles with the following gradation:

The dry loose unit weight shall be less than 50 pounds per cubic feet (pcf). The lightweight aggregate supplier shall submit verification of an in-place compacted total unit weight (by methods defined in AASHTO T99) of less than 65 pcf. For purposes of this specification, the total unit weight is defined as the maximum dry density multiplied by one plus the moisture content (as a decimal). For example, if the maximum dry density is 45 pcf and the moisture content is 9%, the total unit weight is 49 pcf.

The maximum soundness loss when tested with 5 cycles of magnesium sulfate shall be 10 percent (ASTM C 88). The maximum Los Angeles Abrasion loss when tested in accordance with ASTM C 131 (B grading) shall be 40 percent.

The lightweight aggregate producer shall submit verification that the angle of internal friction is equal to or greater than 40 degrees when measured in a triaxial compression test on a laboratory sample with a minimum diameter of 250mm.

The materials for bagged stone shall conform to the following requirements: the crushed stone or gravel shall conform to the grading requirements of Article M.01.01 for No. 3 or No. 4 coarse aggregate or a mixture of both; the bag shall be of burlap and shall be large enough to contain one cubic foot of loosely packed granular material. Construction Methods: When applicable and except where noted below, lightweight fill placement shall conform to the requirements of Sections 2.02.03 and 2.16.03 of the Standard Specifications, Form 817.

The lightweight fill shall be placed in layers of a thickness of 1.5 ft to a maximum of 2.0 ft. Each layer shall be compacted by the use of self-propelled vibratory compaction equipment with static mass (weight) less than 6,600 lbs. The minimum number of passes shall be two (2) and the maximum four (4). The actual lift thickness and exact number of passes shall be determined by the Engineer depending on the type of compaction equipment. The contractor shall take all necessary precautions during construction activities in operations on or adjacent to the lightweight fill to ensure that the material is not over compacted. Construction equipment, other than for compaction, shall not be operated on the exposed lightweight fill.

Where weep holes are installed within the limits of the lightweight fill, bagged stone shall be placed around the inlet end of each weep hole, to prevent movement of the lightweight fill material into the weep hole. Approximately one cubic foot of crushed stone or gravel shall be enclosed in each of the burlap bags. All bags shall then be securely tied at the neck with cord or wire so that the enclosed material is contained loosely. The filled bags shall be stacked at the weep holes to the dimensions shown on the plans or as directed by the Engineer. The bags shall be unbroken at the time lightweight fill material is placed around them and bags which are broken or burst prior to or during the placing of the lightweight fill material shall be replaced at the expense of the contractor.

Method of Measurement: Lightweight fill shall be measured in place after compaction, including allowances for settlement. There shall be no direct payment for bagged stone, but the cost thereof shall be considered as included in the cost of the work for "Lightweight Fill".

Basis of Payment: This work will be paid for at the contract unit price per cubic yard for "Lightweight Fill", complete in place, which price shall include all materials, transportation, tools, equipment and labor incidental thereto.

Pay Item Lightweight Fill **Pay Unit** c.y.

LAND DEVELOPMENT | ENGINEERING DESIGN | CONSTRUCTION SERVICES

Geotechnical Report Rehabilitation of Bridge 06043 Route 15 NB over Main Street State Project No. 63-703 East Hartford, Connecticut

December 22, 2016

Freeman Project No.: 2014-1001

Prepared for: **CME Associates, Inc. 333 East River Drive, Suite 400 East Hartford, CT 06108**

Prepared by:

Freeman Companies, LLC 36 John Street Hartford, CT 06106

> Nathan L. Whetten, P.E., D.GE. Vice President of Geotechnical Services

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- C. Results of Laboratory Testing
- D. Draft Special Provisions

1.0 INTRODUCTION

1.1 Summary

This report presents our evaluation of subsurface conditions and geotechnical engineering recommendations for rehabilitation of Bridge 06043, Route 15 over Main Steet in East Hartford. Rehabilitation consists of widening the northbound (south) side of the bridge by 12 feet to accommodate an additional travel lane. The existing bridge is a single-span bridge supported on two stub abutments, which will be extended to the south. New U-type wingwalls will be provided.

We recommend that the widened abutments be supported on steel H-Piles driven to refusal on bedrock, and pile tip reinforcement should be provided. Filling behind the abutments and new wingwalls will result in settlement of subgrade soils, and downdrag loads on abutment piles will occur. We recommend that bitumen coatings be applied to piles supporting the widened abutment to reduce downdrag loads. Preaugering will be required to protect the coatings.

Abutments should be backfilled with lightweight fill (expanded shale aggregate), consistent with backfill recommended in the original design documents against the existing bridge abutments, to reduce the magnitude of total and differential settlement.

1.2 Scope of Work

Freeman Companies, LLC performed the following tasks:

- Engaged a subsurface exploration contractor to conduct test borings at the site.
- Provided technical monitoring of the explorations.
- Arranged for a testing laboratory to conduct laboratory soil tests.
- Evaluated the subsurface conditions
- Conducted settlement evaluations
- Prepared this report containing geotechnical design recommendations and construction considerations.

1.3 Authorization

The work was completed in accordance with our agreement dated October 21, 2015.

1.4 Project Vertical Datum

Elevations in this report are in feet and reference NAVD-88.

2.0 PROJECT AND SITE DESCRIPTION

2.1 Project Description

The bridge will be widened by 12 feet by extending Abutments 1 and 2 on the south side. New U-type wingwalls will be provided.

The existing bridge is supported on steel H-piles. Design documents for the existing bridge recommended that bitumen coatings be applied to reduce downdrag. Lightweight fill was recommended within 75 feet of the abutments to limit settlement.

2.2 Site Description

The site is located on the south side of the Route 15 NB Bridge over Main Street, as shown on Figure 1, Site Location Map. The bridge is a single-span bridge supported on stub abutments. Main Street has three travel lanes in each direction and concrete sidewalks on each side. The slope between the stub abutments and sidewalks is paved with concrete pavers. Ground surface south of the wingwalls consists of grass and shrubs.

Bridge grade is about El. 61, Main Street grade below the bridge is about El. 37, and bottom of pile cap (existing and proposed) is at El. 43.

3.0 EXPLORATIONS

3.1 Recent Explorations

Recent explorations included one Cone Penetrometer Test (CPT6043-1) and one test boring (S6043-1 OW) conducted on June 15, 2016 and from May 21 to 24, 2016, respectively. The Cone Penetrometer Test (CPT) was conducted by ConeTec, of West Berlin, New Jersey, and the test boring was drilled by New England Boring Contractors, Inc., Glastonbury, Connecticut. CPT6043-1 was located south of Abutment 1 and S6043-1 was located south of Abutment 2.

CPT6043-1 was drilled to a depth of 164.4 feet (CPT6043-1) below ground surface. The CPT was advanced using standard CPT push techniques, and the subsurface data was recorded continuously by a piezocone mounted on the tip.

Test boring S6043-1 was drilled to a depth of 189 feet below ground surface. Standard Penetration Tests at maximum 5 foot intervals, undisturbed tube samples of the lacustrine deposits, and two five-foot-long NX-size rock core samples were recovered from the boring. The completed borehole was backfilled with drill cuttings. A groundwater observation well was installed in a test boring immediately adjacent to S6043-1 drilled to a depth of 20 feet. A slotted PVC screen backfilled with filter sand was placed from 10 to 20 feet. The installation was protected with a roadway box.

A Freeman Companies geologist monitored the drilling, described the soil samples, and prepared the test boring logs included in Appendix A, Recent Exploration Logs. The CPT log prepared by ConeTec is also included in Appendix A. Exploration locations were surveyed by CME Associates, and are shown on Figure 2, Subsurface Exploration Location Plan.

3.2 Previous Subsurface Explorations

Six previous test borings were drilled for the bridge, including B-10, and B-164 to B-168. Approximate locations of borings obtained from record documents are shown on Figure 2, Exploration Location Plan. Previous exploration logs and cross-sections of the previous explorations are provided in Appendix B.

3.3 Laboratory Testing

A laboratory testing program was conducted, consisting of:

- Eight moisture content tests
- One pH test, one electrical resistivity test, and one soluble sulfate test
- One grain size analysis
- Two Constant Rate of Strain (CRS) Consolidation Tests
- Four Atterberg Limit Determinations
- One unconfined compression test on a rock core sample.

Laboratory tests were conducted by Geotesting Express, of Acton, Massachusetts. Results of laboratory testing are provided in Appendix C, Laboratory Test Data. Results of previous and recent consolidation tests are plotted on Figure 3 Summary of Varved Clay Properties, East of Connecticut River.

4.0 SUBSURFACE CONDITIONS

4.1 Subsurface Conditions

Subsurface conditions encountered in the explorations include Fill, Alluvium, Lacustrine, and Glacial Till overlying Bedrock as described below. A summary of subsurface data is provided in Table I. A subsurface profile through Abutment 2 is provided on Figure 4.

Groundwater – Water was encountered in the borings at depths ranging from 11 to 20 feet (El 21 to El. 29) during or shortly after drilling. Groundwater was measured in observation well S6043-1 OW at 10.6 feet (El. 29) 4 months after the well was installed, following a relatively dry period of weather. Groundwater levels will vary with season, water level in the nearby Connecticut River, precipitation, temperature, and other factors.

Corrosion – One series of corrosion tests was conducted on a sample from boring S6043-1. Results of testing are summarized below:

Results of testing indicate the sample is non-corrosive based on guidance provided in AASHTO Section 10.7.5.

5.0 GEOTECHNICAL ENGINEERING RECOMMENDATIONS

5.1 Foundation Design Recommendations

Downdrag – Settlement evaluations were conducted at the proposed abutments to estimate the magnitude of total settlement, and whether settlement would cause downdrag at the existing and proposed piles. Estimated total settlement calculated at the abutments assuming various weights of fill, calculated using the computer program Settle 3D (by RocScience), is summarized as follows:

Results of the evaluation indicate that there is on-going settlement of the existing embankment from the original embankment fill loads, both consolidation settlement and secondary compression. Additional fill loads using either normal weight fill or a super-lightweight material such as geofoam have a limited impact on the magnitude of settlement.

The threshold settlement for downdrag loads on piles is commonly considered to be 0.4 inches. The estimated settlements will result in downdrag loads on the abutment piles. We recommend that bitumen coatings be applied to piles to reduce downdrag loads. A 90 percent reduction in downdrag loads can be achieved using bitumen coatings, provided that coatings are protected from damage during pile installation. Coated piles should be installed in a preaugered and cased hole to avoid damage to the piles during pile driving. Sand should be placed around the pile as the casing is withdrawn.

Settlement evaluations indicate that there is not a significant reduction in settlement by using geofoam. The original design recommendations called for lightweight backfill (expanded shale aggregate) within 75 feet of the bridge abutment. We recommend that backfill adjacent to the widened portions of the bridge also consist of expanded shale aggregate, consistent with the original design recommendations, to reduce the magnitude of differential settlement.

Pile Design

- **Seismic Design:** Soils are not susceptible to liquefaction. Soil conditions at the site are defined as AASHTO Site Class D, Stiff Soils.
- **Pile Type:** HP12x74 with pile tip reinforcement driven to end bearing on bedrock, Grade 50 steel. Other H-Pile sections may also be considered.
- **Service Limit:** 125 tons, assumes a HP12x74 pile area equal to 21.76 square inches. Reduce the capacity to account for downdrag loads on piles supporting the abutments, as indicated below.
- **Strength Limit:** For end bearing piles, assume a strength limit equal to the structural capacity of the pile.
- Settlement of piles is expected to be equal to the elastic compression of the pile.
- **Downdrag:** Estimated downdrag loads are listed below:
	- 350 tons (single piles, uncoated) or 35 tons (single pile with bitumen coating)
	- 31.5 tons (corner pile in a group with bitumen coating)
	- 28 tons (side pile in a group with bitumen coating)
	- 17.5 tons (inside pile in a group with bitumen coating)
- **Load Tests:** Minimum of 3 dynamic load tests with matching signal analysis (4 tests if 26 or more piles, and no less than 2% of the production piles, AASHTO Table 10.5.5.2.3-3).
- **Test Piles:** Recommend same piles and criteria as load tests (AASHTO 10.7.9)
- • **Minimum Spacing:** Center to center spacing should be 2½ times the pile diameter (AASHTO 2012 10.7.1.2) and at least 30 inches. Minimum 9 inches to the nearest edge of the pile cap
- • **Lateral Resistance:** Use the pile capacity in batter. Additional lateral load capacities in bending will be provided based on LPile analyses once pile loading is established.
- **Subgrade Preparation Below Pile Cap:** Minimum 12-inch thick layer of Granular Fill (CTDOT Form 817 M.02.01) over the subgrade.
- **Bottom of Structure and Estimated Pile Tip Elevations:**

Abutment Design

6.0 CONSTRUCTION CONSIDERATIONS

6.1 Excavation

Conventional excavation equipment appears practical for excavation. Excavation geometries should conform to OSHA excavation regulations contained in 29 CFR 1926, latest edition.

6.2 Pile Installation

The maximum hammer energy should be determined by a wave equation analysis by the contractor based on the specific hammer characteristics. Test piles and dynamic load testing should be conducted as indicated above. Vibrations from pile driving should not affect the structural integrity of adjacent structures. However, vibration and noise will likely be noticeable inside buildings 300 feet away, or more.

Where bitumen coats are required, coatings should be applied to the piles prior to transportation to the site. It should include a primer coat that may be sprayed or painted onto the piles, and a final coat.

Piles with bitumen should be installed in a preaugered and cased hole to avoid damage to the piles during pile driving. Piles should be preaugered through the existing fill and alluvial deposits (granular soils) to the top of lacustrine deposits. The top of lacustrine deposits is typically about El 20. Sand should be placed inside the casing as the casing is extracted. Draft special provisions are provided in Appendix D.

6.3 Pile Cap Bearing Surface Preparation

Excavated subgrades for the pile cap should be covered with Granular Fill and then proofrolled with a vibratory plate compactor. If the subgrade beneath the Granular Fill is found to be excessively soft or yielding, it may be necessary to overexcavate the soft material and place additional Granular Fill or crushed stone over separation fabric. If vibratory proof compaction of the subgrade proves detrimental due to the presence of groundwater, static rolling may be allowed at the discretion of the Engineer.

Soil bearing surfaces should be protected against freezing both before and after concrete placement. If construction takes place during winter months, foundations should be backfilled as soon as possible following construction. Alternatively, insulating blankets or other methods may be used to protect against freezing.

6.4 Expanded Shale Aggregate

Expanded shale aggregate should be placed in layers 1.5 to 2 feet thick, and compacted with self-propelled vibratory compaction equipment with static weight less than 6,600 lbs. The minimum number of passes should be limited to two and the maximum four, to avoid particle breakdown during compaction. A draft special provision is included in Appendix D.

6.5 Temporary Lateral Support

We estimate that excavations will be required to reach the pile cap subgrade. Temporary lateral support of excavations will be required to maintain and protect traffic flow, and to protect nearby utilities. Steel sheetpiling or

soldier piles and lagging with multiple levels of bracing appears feasible. Surface water should be diverted away from excavations.

6.6 Excavation Dewatering

Excavation dewatering will be required to permit construction in in-the-dry. Pumping from sumps located in the bottom of excavations appears feasible. Surface water should be diverted away from excavations. Pumping, handling, and treatment of excavation dewatering fluids should be in accordance with all applicable regulatory agency requirements.

6.7 Reuse of Existing Soils

The existing soils to be excavated will consist primarily of fill and silty sands with gravel. These soils are silty and are not expected to be suitable for reuse as Pervious Structure Backfill or Granular Fill. Excavated soils may be suitable for reuse as embankment fill. However the silty soils are difficult to properly compact when wet, and may need to be dried to achieve compaction. Drying the soils can be difficult and at times impractical, particularly during periods of cold and wet weather.

7.0 FUTURE SERVICES AND LIMITATIONS

We recommend that a qualified geotechnical engineer be engaged during construction to observe:

- Preparation of foundation bearing surfaces.
- Pile installation and load tests.
- Verify that soil conditions exposed in excavations are in general conformance with design assumption, and that the geotechnical aspects of construction are consistent with the project specifications.

This report was prepared for the exclusive use of CME Associates and the project design team. The recommendations provided herein are based on the project information provided at the time of this report and may require modification if there are any changes in the nature, design, or location of the structure.

The recommendations in this report are based in part on the data obtained from the subsurface explorations. The nature and extent of variations between explorations may not become evident until construction. If variations from the anticipated conditions are encountered, it may be necessary to revise the recommendations in this report.

Our professional services for this project have been performed in accordance with generally accepted engineering practices; no warranty, expressed or implied, is made.

2014-1001 Rehabilitation of Route 15 over Main Street Contract CORE ID: 15DOT0148AA, State Project No. 63-703 East Hartford, Connecticut

Table 1 Subsurface Data

Notes:

1. Ground surface elevations at recent test borings were surveyed by CME Associates, Inc. Ground surface elevation at previous borings were shown on the logs and corrected to NAVD-88 on this table.

2. Groundwater levels are approximate. See S6043-1 OW log for date of water level measurement in observation well.

3. Top of bedrock is inclusive of weathered rock

4. ">" - Greater Than "--" - Not Encountered (C) - Bedrock Core Taken (R) - Terminated at Refusal "NM" - Not Measured

FIGURES

THESE DRAWINGS SHALL NOT BE UTILIZED BY ANY PERSON, FIRM OR CORPORATION WITHOUT THE SPECIFIC WRITTEN PERMISSION OF FREEMAN COMPANIES, LLC

NOTES

- **DEFINITIONS**
- COMPRESSION RATIO $(=\Delta \varepsilon / \Delta \log \sigma'_{V})$ DURING VIRGIN COMPRESSION **CR** $\qquad \qquad$
- RECOMPRESSION RATIO $(=\Delta \varepsilon / LOG\sigma'_{V})$ during recompression **RR**
- σ'νο IN SITU VERTICAL EFFECTIVE STRESS
- PRECONSOLIDATION STRESS σ_{P} $\overline{}$

OAK BRIDGE AND APPROACHES, HARTFORD-EAST HARTFORD, CONNECTICUT" DATED MAY 1987.

TITLED "GEOTECHNICAL LABORATORY DATA REPORT, CHARTER

1. PREVIOUS DATA WAS OBTAINED FROM THE RECORD REPORT

2. ELEVATIONS REFER TO NAVD-88. PREVIOUS ELEVATIONS WERE ADJUSTED FROM NGVD-29.

SUMMARY OF VARVED CLAY PROPERTIES **EAST OF CONNECTICUT RIVER** STATE PROJECT NO. 63-703 HARTFORD, CONNECTICUT **FIGURE 3B**

M.K. $N.W.$ N.W.

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APPENDIX A

RECENT EXPLORATION LOGS

The reported coordinates were acquired from consumer-grade GPS equipment and are only approximate locations. The coordinates should not be used for design purposes.

APPENDIX B

PREVIOUS TEST BORING LOGS

FIGURE 3

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Contract Contract

ABUTMENT NO.I.

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ABUTMENT NO. 2

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STRUCTURE NO. 2 ROUTE 15 OVER MAIN STREET

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TABLE I SUMMARY OF FIELD VANE SHEAR TEST RESULTS

Notes:

(1) Su = Shear Strength
(2) Sensitivity = Undisturbed/molded shear strength
(3) See Table II for Vane Dimensions

APPENDIX C

RESULTS OF LABORATORY TESTING

Moisture Content of Soil and Rock - AASHTO T 265

Notes: Temperature of Drying : 110º Celsius

Moisture Content of Soil and Rock - AASHTO T 265

pH of Soil by ASTM D4972

Notes: Sample Preparation: screened through #10 sieve Method A, pH meter used

Laboratory Measurement of Soil Resistivity Using the Wenner Four-Electrode Method by ASTM G57 (Laboratory Measurement)

Notes: Test Equipment: Nilsson Model 400 Soil Resistance Meter, MC Miller Soil Box Water added to sample to create a thick slurry prior to testing (saturated condition). Electrical Conductivity is calculated as inverse of Electrical Resistivity (per ASTM G57) Test conducted in standard laboratory atmosphere: 68-73 F

FUGRO CONSULTANTS, INC.

 PHONE (713) 369-5400 FAX (713) 369-5518

THE RESULTS RELATE AS TO THE LOCATION TESTED AND NO OTHER REFERENCE SHALL BE MADE.

THIS REPORT SHALL NOT BE REPRODUCED EXCEPT IN FULL WITHOUT THE WRITTEN APPROVAL OF THE LABORATORY.

VACUUME FILTRATION. THE WATER EXTRACT IS THEN ANALYZED USING THE ASTM D-512 AND D-516 METHODS.

**** WATER EXTRACTION PERFORMED BY USING A 1:10 RATIO OF SAMPLE AND REAGENT WATER FOLLOWED BY CENTRIFUGE AND**

 (GTX 304831) CLIENT NUMBER: JOB NUMBER: 04.1115-0003 FOR: **GEOTESTING EXPRESS, INC. REPORT NUMBER:** 125 NAGOG PARK ACTION, MA 01720 DATE SAMPLED: **TIME SAMPLED: REPORTED TO: ETHAN MARRO SAMPLED BY: CLIENT DATE RECEIVED: TIME RECEIVED:** SOLUBLE SULFATE AASHTO T-290 RECEIVED BY: SAMPLE ID | RESULTS | UNITS | LAB No. | TIME/DATE | ANALYST S1-S, S-2, 4 – 6' \vert < 30 \vert + \vert mg/kg \vert 0726052 1100/08-01-16 SD S1-5, S-3, 10 – 12' | 57 * | mg/kg | 0726053 | 1100/08-01-16 | SD S1-12, S-2, 5 – 7' \vert $<$ 50 * | mg/kg | 0726054 | 1100/08-01-16 | SD S2-1, S-4, 15 – 17' < 50 * mg/kg 0726055 1100/08-01-16 SD S2-3, S-2, 5 – 7' | 297 * | mg/kg | 0726056 | 1100/08-01-16 | SD S-0480-1, S-5, 14 – 16' | 543 * | mg/kg | 0726057 | 1100/08-01-16 | SD

S-0480-2, S-3, 9 – 11' 355 * mg/kg 0726058 1100/08-01-16 SD S-06043-41, S-2, 5 – 7' < 30* mg/kg 0726059 1100/08-01-16 SD

SO4CL 069-16

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Respectfully submitted,

*** Dry weight basis**

6100 HILLCROFT HOUSTON, TEXAS 77081

REPORT DATE: 08-01-16

RESULTS OF TESTS

Steve DeGregorio Chemist

SD

PROJECT: RECONSTRUCTOION OF EXIT CHARTER OAK BRIDGE

Sample/Test Description Sand/Gravel Particle Shape : ---

Sand/Gravel Hardness : ---

Sample Prepared using the WET method

Sample Prepared using the WET method

Sample Prepared using the WET method

Sample Prepared using the WET method

Constant Rate of Consolidation

Constant Strain Rate by ASTM D4186

Summary Report

Constant Rate of Consolidation Constant Strain Rate by ASTM D4186 Pressure Curves

CRC TEST DATA

Soil Description: Moist, dark gray clay Remarks: System Y

Note: Specific Gravity and Void Ratios are calculated assuming the degree of saturation equals 100% at the end of the test. Therefore, values may not represent actual values for the specimen.

Constant Rate of Consolidation

Constant Strain Rate by ASTM D4186

Summary Report

Constant Rate of Consolidation Constant Strain Rate by ASTM D4186 Pressure Curves

Note: Specific Gravity and Void Ratios are calculated assuming the degree of saturation equals 100% at the end of the test. Therefore, values may not represent actual values for the specimen.

Bulk Density and Compressive Strength of Rock Core Specimens by ASTM D7012 Method C

Notes: Density determined on core samples by measuring dimensions and weight and then calculating.

All specimens tested at the approximate as-received moisture content and at standard laboratory temperature.

The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.

Failure Type: 1 = Intact Material Failure; 2 = Discontinuity Failure; 3 = Intact Material and Discontinuity Failure (See attached photographs)

- 1: Best effort end preparation. See Tolerance report for details.
- 2: The as-received core did not meet the ASTM side straightness tolerance due to irregularities in the sample as cored. 3: Specimen L/D < 2.
- 4: The as-received core did not meet the ASTM minimum diameter tolerance of 1.875 inches.
- 5: Specimen diameter is less than 10 times maximum particle size.
- 6: Specimen diameter is less than 6 times maximum particle size.

*Because the indicated tested specimens did not meet the ASTM D4543 standard tolerances, the results reported here may differ from those for a test specimen within tolerances.

UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO ASTM D4543

APPENDIX D

DRAFT SPECIAL PROVISIONS

ITEM #0702081A- BITUMINOUS COATING FOR STEELPILES

Description: Work under this item shall consist of furnishing and applying bituminous coating to steel piles. This work shall be performed as hereinafter specified, to the dimensions indicated on the plans, or as directed by the Engineer. This work shall also include field applied touch ups to coating damaged during shipping and handling.

Materials: Provide bituminous coating for all piles. Bituminous coating shall consist of canal liner bituminous in accordance with ASTM D 2521. It shall have a softening point of 190°F to 200°F a penetration of 56 to 61 at 77°F and a ductility in excess of 1.38 in. at 77°F. Primer shall be in accordance with AASHTO M 116.

Construction Methods:

- A. All surfaces to be coated with bituminous shall be dry and thoroughly cleaned of dust and loosematerials.
- B. Primer or bituminous shall not be applied in wet weather, nor when the ambient temperature is below65°F.
- C. Application of the prime coat shall be with a brush or other approved means and in a manner which thoroughly coats the surface of the piling with a continuous film of primer. The primer shall have set thoroughly before the bituminous coating is applied. The bituminous shall be heated to 300°F and applied at a temperature between 200° and 300°F by means of one or more mop coats or other approved means.
- D. The average coating thickness shall be 1/16".
- E. Whitewashing of the coating may be required during hot weather as directed to prevent running or sagging of the asphalt coating prior to driving of the pile.
- F. Bituminous coated piles shall be protected from sunlight or heat immediately after the coating is applied.
- G. The bituminous coating shall not be exposed to damage or contamination during storage, hauling, or handling. Once the bituminous coating has been applied, dragging the piles on the ground or the use of cable wraps around the piles during handling will not be permitted. Pad eyes, or other suitable devices, shall be attached to the piles to be used for lifting and handling.
- H. Where Field splices are required the bituminous coating shall be removed in the splice area. After completing the field splice, the splice area shall be brush coated or mop coated with a minimum of one coat of bituminous material as directed.

Method of Measurement: Bituminous coating will be measured per linear foot of pile coated.

Basis of Payment: Payment shall be made at the contract unit price per linear foot of pile coated. This price shall be full compensation for furnishing all materials, for preparing and placing these materials, and for all labor, equipment tools, and incidentals necessary to complete

ITEM #0702081A

ITEM #0702109A- PRE-AUGERING OF PILES

ITEM #0702111A- DRIVING STEEL PILES

Work under this item shall conform to the requirements of Section 7.02 of Form 817 as replaced by the special provision for Section 7.02 in this contract, amended as follows:

7.02.01- Description: Add the following:

Work under this Item includes pre-augering for piles as indicated on the Plans or as ordered by the Engineer.

7.02.03.2(a) - Construction Methods - Pile Driving Equipment - Hammers: Replace the second paragraph with the following:

The size of hammer shall be adapted to the type and size of piles and the driving conditions. Unless otherwise specified, the minimum rated striking energy per blow for hammers used shall be 26,000-foot pounds (35,000 joules) for driving steel piles. The hammer model used for the driving of test piles shall be used for the driving of service or production piles, unless a change is authorized by the Engineer in writing. Hammers delivering an energy which the Engineer considers detrimental to the piles shall not be used.

7.02.03.2(7) - Construction Methods - Pile Driving Equipment - Pre-Augering: Add the following:

The following apply when pre-auguring is done for piles with bituminous and epoxy coating:

The pre-augered hole is to continue to the top of the clay layer or to the depths shown on the plans or as directed by the Engineer. The pre-augered hole diameter shall be at least the diagonal dimension of the pile, or as directed by the Engineer. All obstructions which could interfere with the driving of piles within the depth of pre-augering are to be removed as part of the pre-auguring work.

The Contractor shall provide temporary casing to maintain the pre-augured dimension of the hole. Upon completion of pile driving, the annulus between the pile and outer hole diameter shall be filled with clean sand and any temporary casing will be removed.

7.02.05.11 - Basis of Payment - Pre-Augering of Piles: Add the following:

This work shall also include obstruction removal, casing, and sand backfill

11/4/14

ITEM #0207150A - LIGHTWEIGHT FILL

Description: Work shall consist of furnishing and placing lightweight fill in the formation of embankments or as backfill in front of and behind structures. This work shall be performed as hereinafter specified, to the dimensions indicated on the plans, or as directed by the Engineer. This item shall also consist of furnishing and placing crushed stone or gravel in burlap bags at the inlet ends of weep holes in structures to the dimensions indicated on the plans or as ordered by the Engineer.

Materials: Lightweight fill shall be a rotary kiln expanded shale aggregate meeting the requirements of ASTM C 330. No by-product slags, cinders or by-products of coal combustion shall be permitted. The aggregate shall consist of tough, durable, non-corrosive particles with the following gradation:

The dry loose unit weight shall be less than 50 pounds per cubic feet (pcf). The lightweight aggregate supplier shall submit verification of an in-place compacted total unit weight (by methods defined in AASHTO T99) of less than 65 pcf. For purposes of this specification, the total unit weight is defined as the maximum dry density multiplied by one plus the moisture content (as a decimal). For example, if the maximum dry density is 45 pcf and the moisture content is 9%, the total unit weight is 49 pcf.

The maximum soundness loss when tested with 5 cycles of magnesium sulfate shall be 10 percent (ASTM C 88). The maximum Los Angeles Abrasion loss when tested in accordance with ASTM C 131 (B grading) shall be 40 percent.

The lightweight aggregate producer shall submit verification that the angle of internal friction is equal to or greater than 40 degrees when measured in a triaxial compression test on a laboratory sample with a minimum diameter of 250mm.

The materials for bagged stone shall conform to the following requirements: the crushed stone or gravel shall conform to the grading requirements of Article M.01.01 for No. 3 or No. 4 coarse aggregate or a mixture of both; the bag shall be of burlap and shall be large enough to contain one cubic foot of loosely packed granular material. Construction Methods: When applicable and except where noted below, lightweight fill placement shall conform to the requirements of Sections 2.02.03 and 2.16.03 of the Standard Specifications, Form 817.

The lightweight fill shall be placed in layers of a thickness of 1.5 ft to a maximum of 2.0 ft. Each layer shall be compacted by the use of self-propelled vibratory compaction equipment with static mass (weight) less than 6,600 lbs. The minimum number of passes shall be two (2) and the maximum four (4). The actual lift thickness and exact number of passes shall be determined by the Engineer depending on the type of compaction equipment. The contractor shall take all necessary precautions during construction activities in operations on or adjacent to the lightweight fill to ensure that the material is not over compacted. Construction equipment, other than for compaction, shall not be operated on the exposed lightweight fill.

Where weep holes are installed within the limits of the lightweight fill, bagged stone shall be placed around the inlet end of each weep hole, to prevent movement of the lightweight fill material into the weep hole. Approximately one cubic foot of crushed stone or gravel shall be enclosed in each of the burlap bags. All bags shall then be securely tied at the neck with cord or wire so that the enclosed material is contained loosely. The filled bags shall be stacked at the weep holes to the dimensions shown on the plans or as directed by the Engineer. The bags shall be unbroken at the time lightweight fill material is placed around them and bags which are broken or burst prior to or during the placing of the lightweight fill material shall be replaced at the expense of the contractor.

Method of Measurement: Lightweight fill shall be measured in place after compaction, including allowances for settlement. There shall be no direct payment for bagged stone, but the cost thereof shall be considered as included in the cost of the work for "Lightweight Fill".

Basis of Payment: This work will be paid for at the contract unit price per cubic yard for "Lightweight Fill", complete in place, which price shall include all materials, transportation, tools, equipment and labor incidental thereto.

Pay Item Lightweight Fill **Pay Unit** c.y.